

# **ESTIMATION OF EFFECTIVE DENSITY AND FRACTAL – LIKE DIMENSION OF SOOT PARTICLES**

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**8<sup>th</sup> ETH-Conference on Combustion Generated Particles  
Zurich 16-18 August 2004**

## MOTIVATION

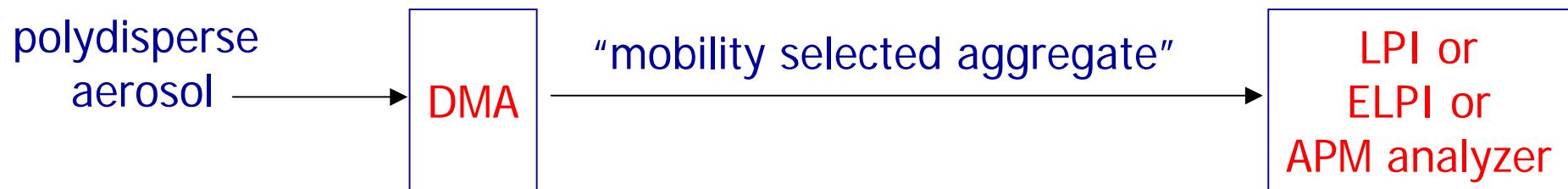
**Structure of combustion generated aggregates is  
important for a number of applications**

- Particulate filters (filtration, pressure drop, reactivity of soot cakes)
- Health effects of soot particles (transport, deposition, interaction with tissues)
- Interactions of soot particles with atmospheric constituents
- Performance of carbon black based products

## MEASUREMENT METHODS FOR SOOT PARTICLE STRUCTURE

- Tandem mobility-aerodynamic or mobility-mass measurements

Skills et al. (1998), Maricq et al. (2000), Park et al. (2003), Van Gulijk et al. (2004),  
Maricq & Xu (2004)



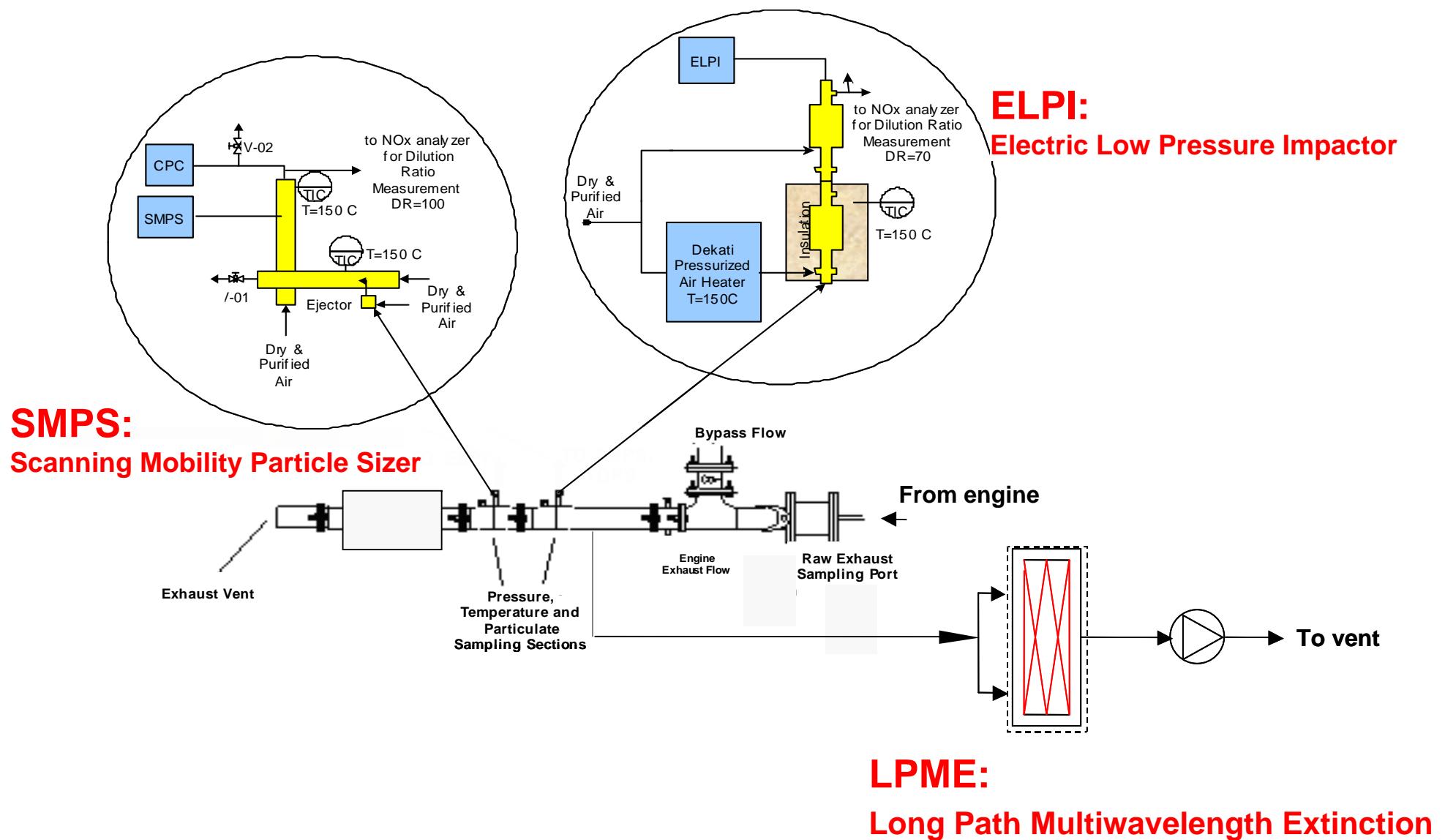
- Parallel application of SMPS and ELPI and matching the two distributions

Ristimaaki et al (2002), **Present work**

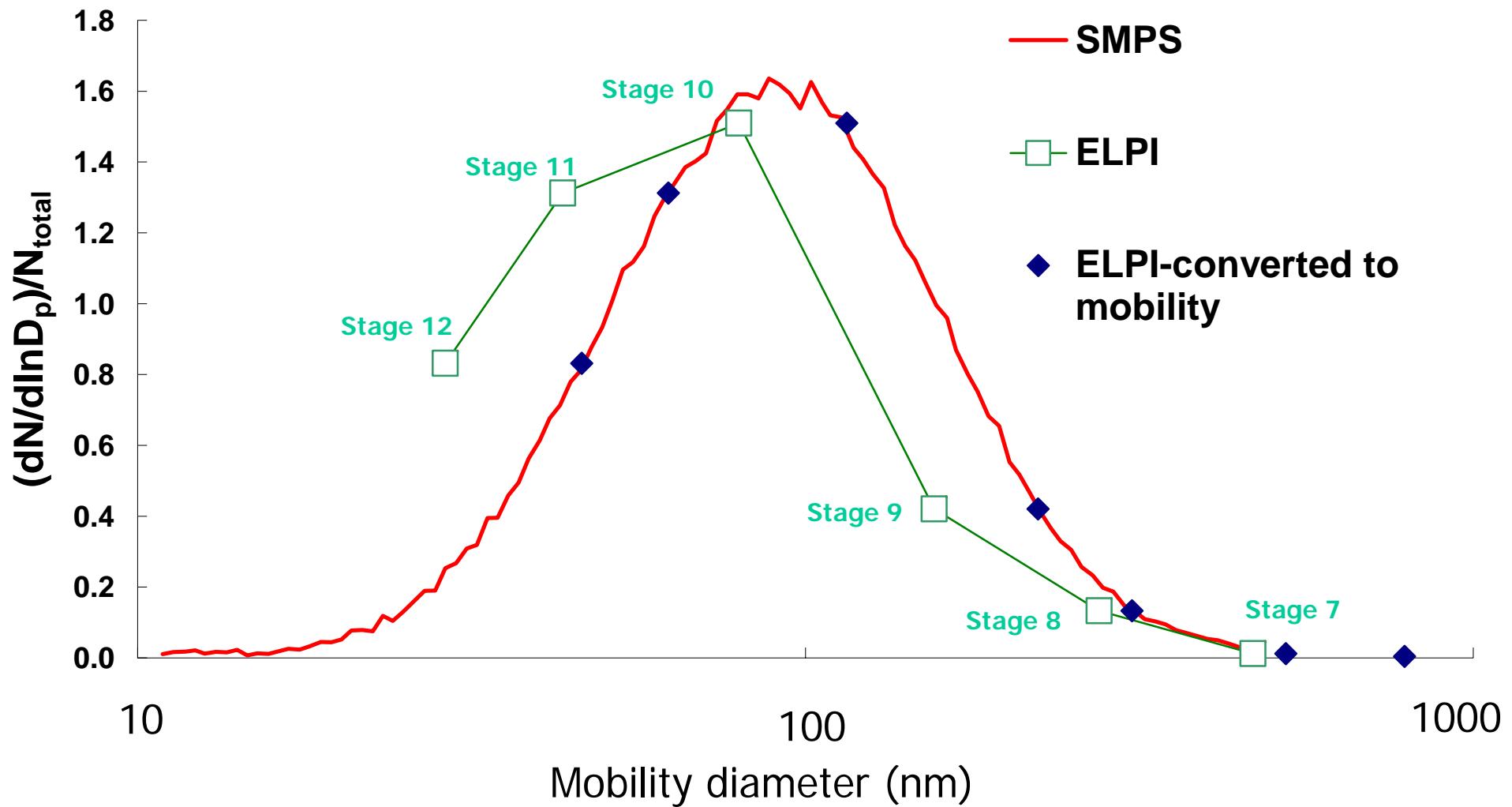
- Optical methods and microscopy

Sorensen and co-workers (1995-2004), di Stasio et al. (1999-2004)

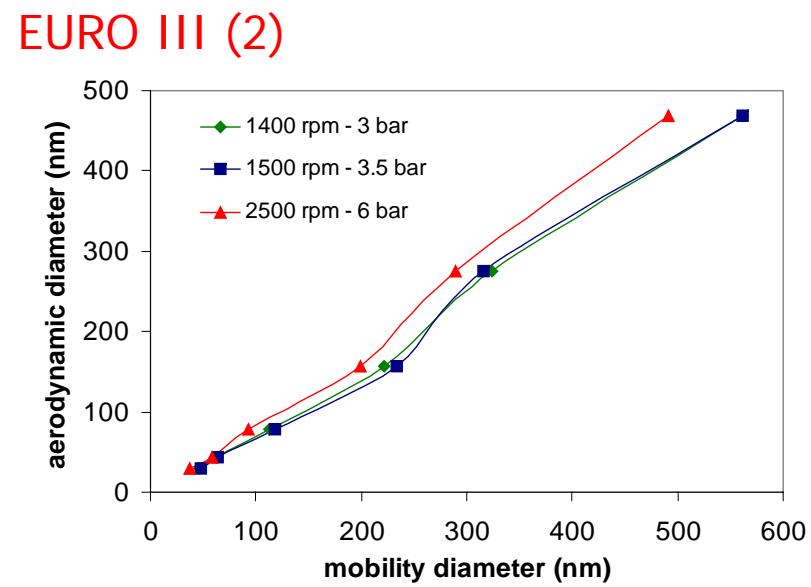
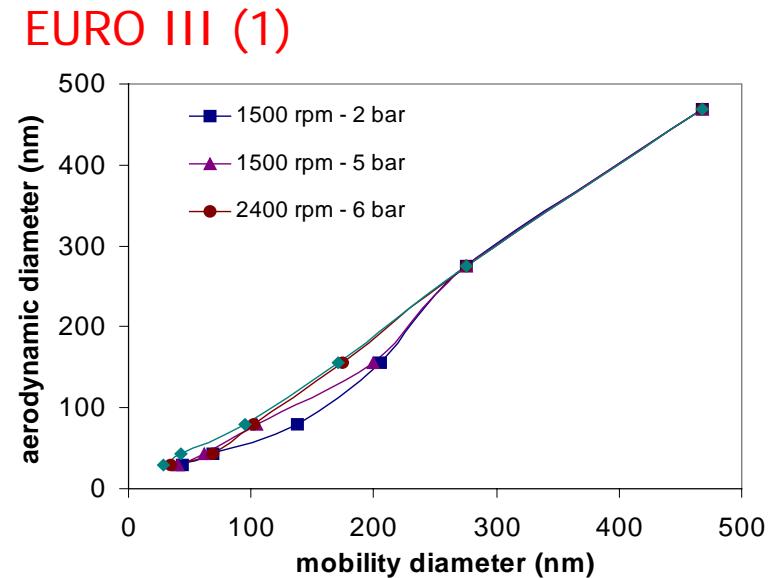
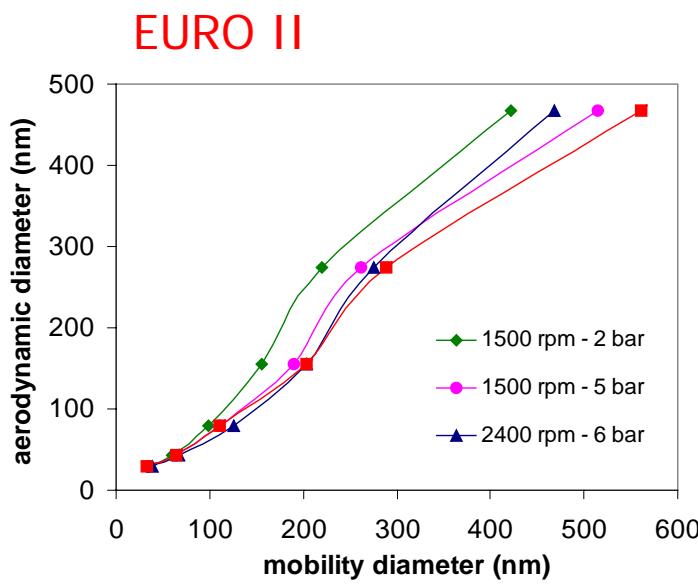
# PARTICLE MEASUREMENT SETUP



## AERODYNAMIC vs. MOBILITY DIAMETER



# AERODYNAMIC vs. MOBILITY DIAMETER FOR 3 PASSENGER CAR DIESEL ENGINES



## DIESEL SOOT FRACTAL AGGREGATES: Definitions

Density and size of primary particles

$\rho_0 \approx 2150 \text{ kg/m}^3$  (CV 20%) based on gravimetry vs. LPME

$d_0 \approx 32 \text{ nm}$  (CV 20%) based on soot cake permeability and TEM

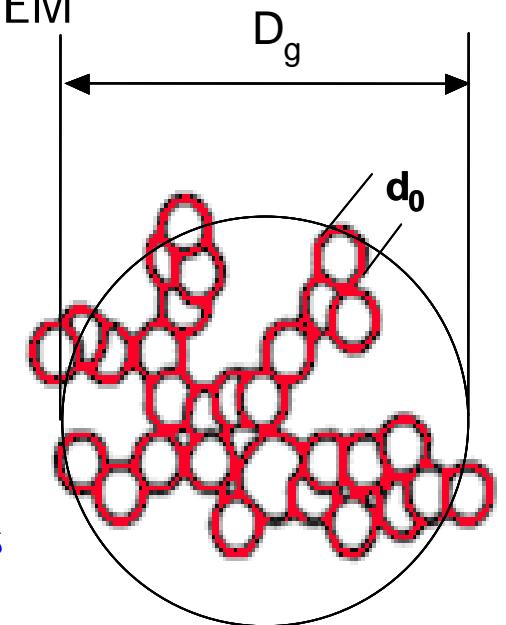
Number of primary particles per aggregate

$$N_A = k_g \left[ \frac{D_g}{d_0} \right]^{D_f}$$

$$k_g = \frac{1}{f} \left[ \frac{D_f}{D_f + 2} \right]^{\frac{D_f}{2}}$$

volume filling factor, Naumann (2003)  $f \approx 1.43$

$D_f \approx 2.4$  on the average Kittelson & McMurry (2002) and others



Geometric diameter

$$\frac{D_{geo}}{d_0} = \left[ f N_A \right]^{\frac{1}{D_f}}$$

Diameter of gyration

$$D_g = \left[ \frac{D_f}{D_f + 2} \right]^{\frac{1}{2}} D_{geo}$$

Mass equivalent diameter

$$\frac{D_{geo}}{d_0} = \left[ \left[ f \left( \frac{D_{mass}}{d_0} \right)^3 \right]^{\frac{1}{D_f}} \right]$$

## MOBILITY DIAMETER OF FRACTAL AGGREGATES

$$D_{me} = h_{KR} D_{geo} = (-0.06483 D_f^2 + 0.6353 D_f - 0.4898) D_{geo}$$

$h_{KR}$  : Kirkwood – Riseman ratio accounting for shielding effects and hydrodynamic interactions

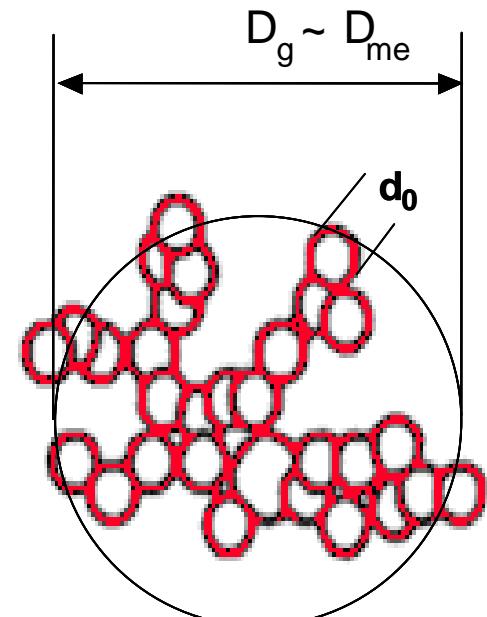
Nauman (2003)

Gyration diameter  $\sim$  Mobility diameter

$$D_g = \left[ \frac{D_f}{D_f + 2} \right]^{\frac{1}{2}} \frac{D_{me}}{h_{KR}}$$

Fractal scaling based on Mobility diameter

$$N_A = k_g \left[ \frac{D_g}{d_0} \right]^{D_f} = k_m \left[ \frac{D_{me}}{d_0} \right]^{D_f}$$



## EFFECTIVE DENSITY OF AGGREGATES

$$\rho_{\text{eff}} D_{me}^2 C_c(D_{me}) = \rho_1 D_{ae}^2 C_c(D_{ae})$$

$\rho_{\text{eff}}$  : effective density

$D_{me}$  : mobility diameter

$\rho_1$  : unit density (1 g/cm<sup>3</sup>)

$D_{ae}$  : aerodynamic diameter

$C_c$ : Stokes-Cunningham Factor

Basic equations of analysis

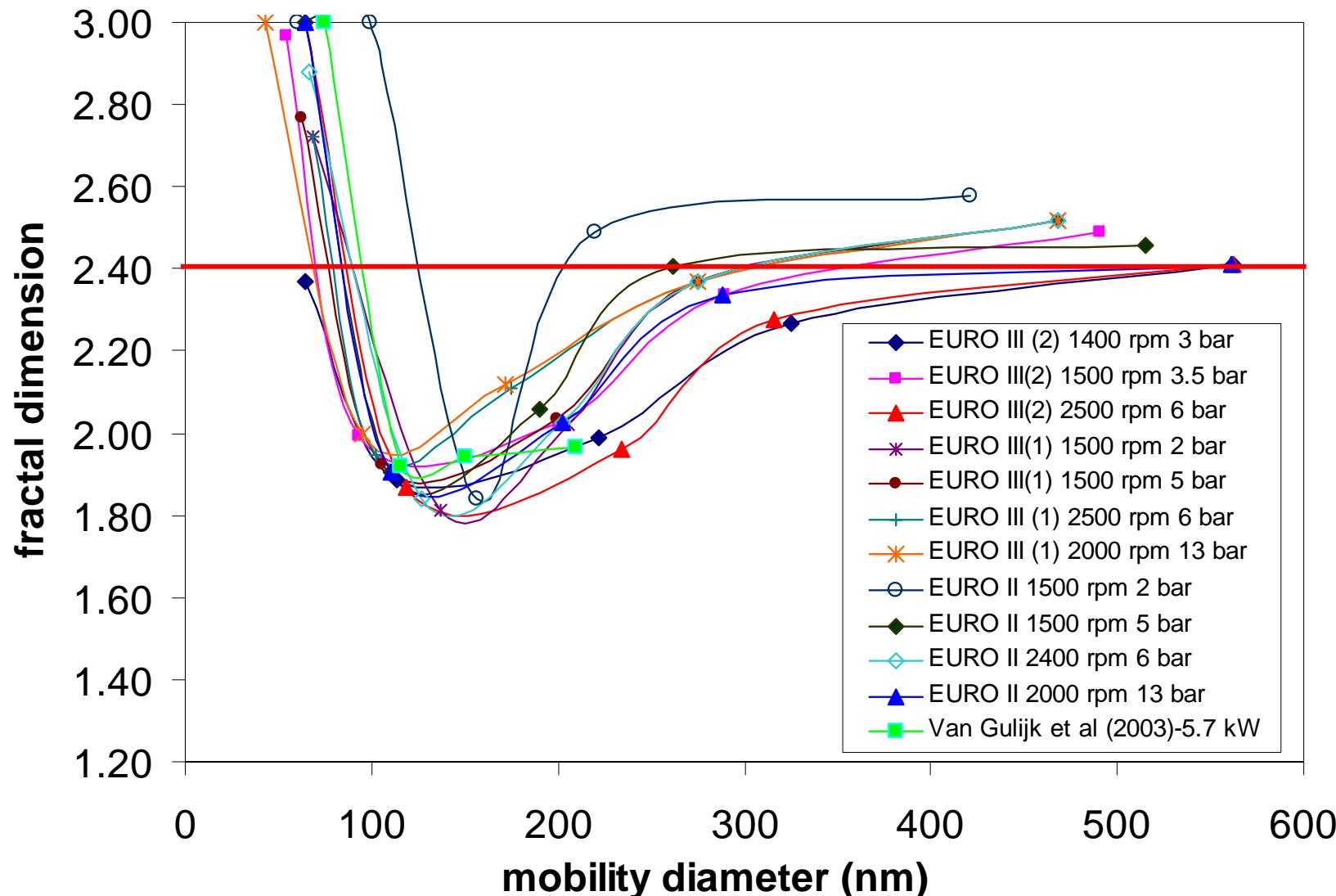
$$\frac{\rho_0}{\rho_1} = \frac{D_{ae}^2 C_c(D_{ae}) f h_{KR}^{D_f}}{D_{me}^{D_f-1} d_0^{3-D_f} C_c(D_{me})}$$

$$\frac{\rho_{\text{eff}}}{\rho_0} = \frac{1}{f h_{KR}^{D_f}} \left[ \frac{D_{me}}{d_0} \right]^{D_f-3}$$

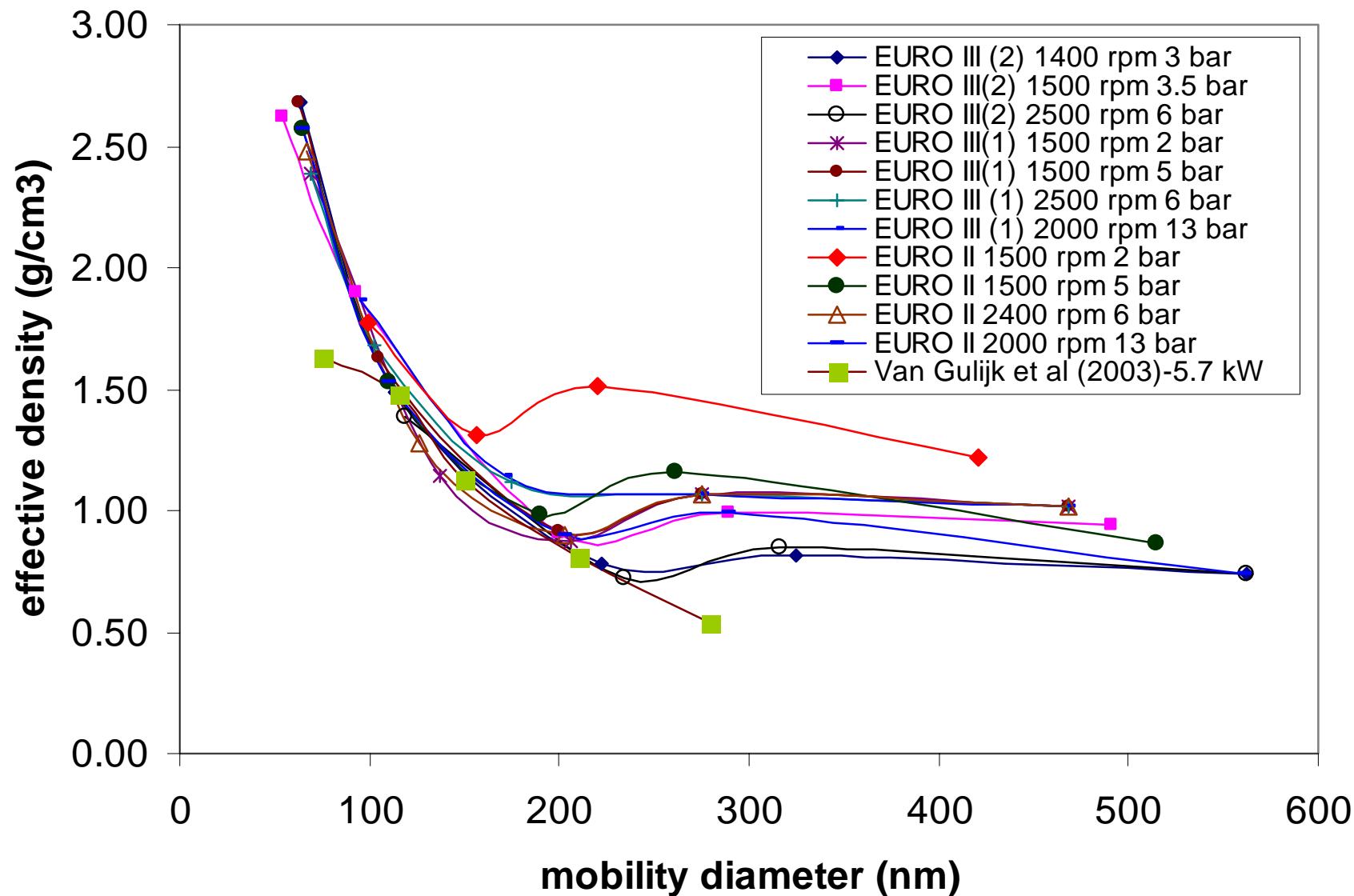
$D_f$

# DIESEL SOOT AGGREGATE FRACTAL DIMENSION

3 different diesel engines & 1 gen set

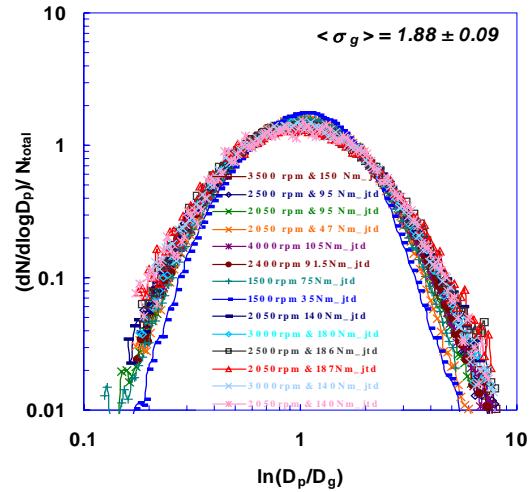


# DIESEL SOOT AGGREGATE EFFECTIVE DENSITY

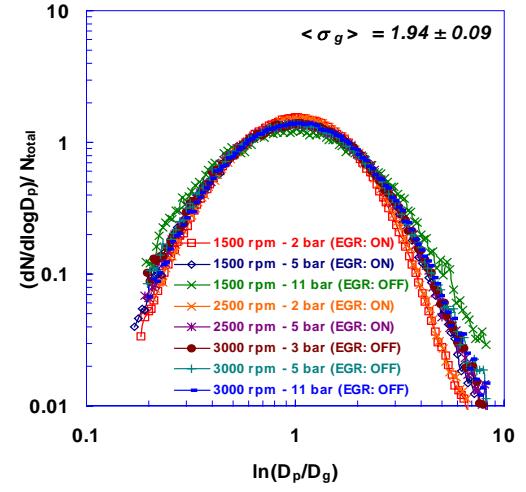


# Diesel aggregate size distribution: 5 Engines (1996-2003) with engine displacement 1.9-2.4 litres

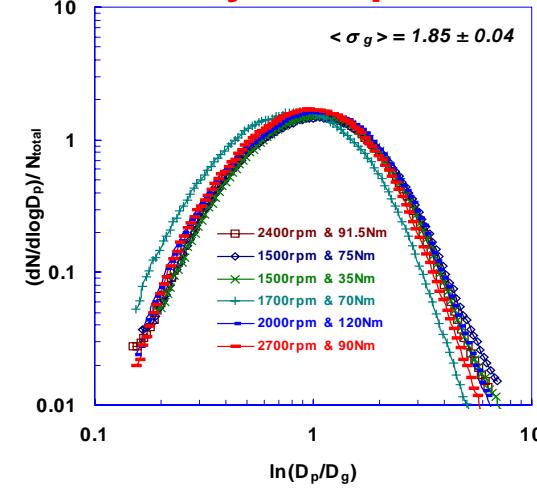
**Common Rail – 1**



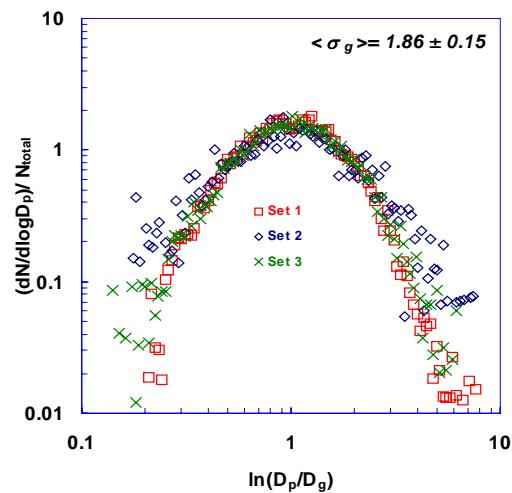
**Common Rail-2**



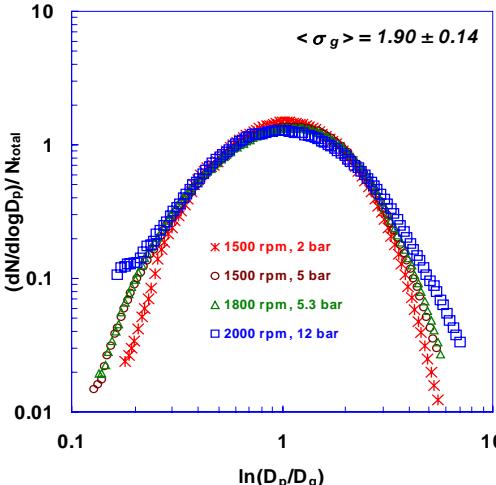
**Rotary Pump**



**Common Rail-3**



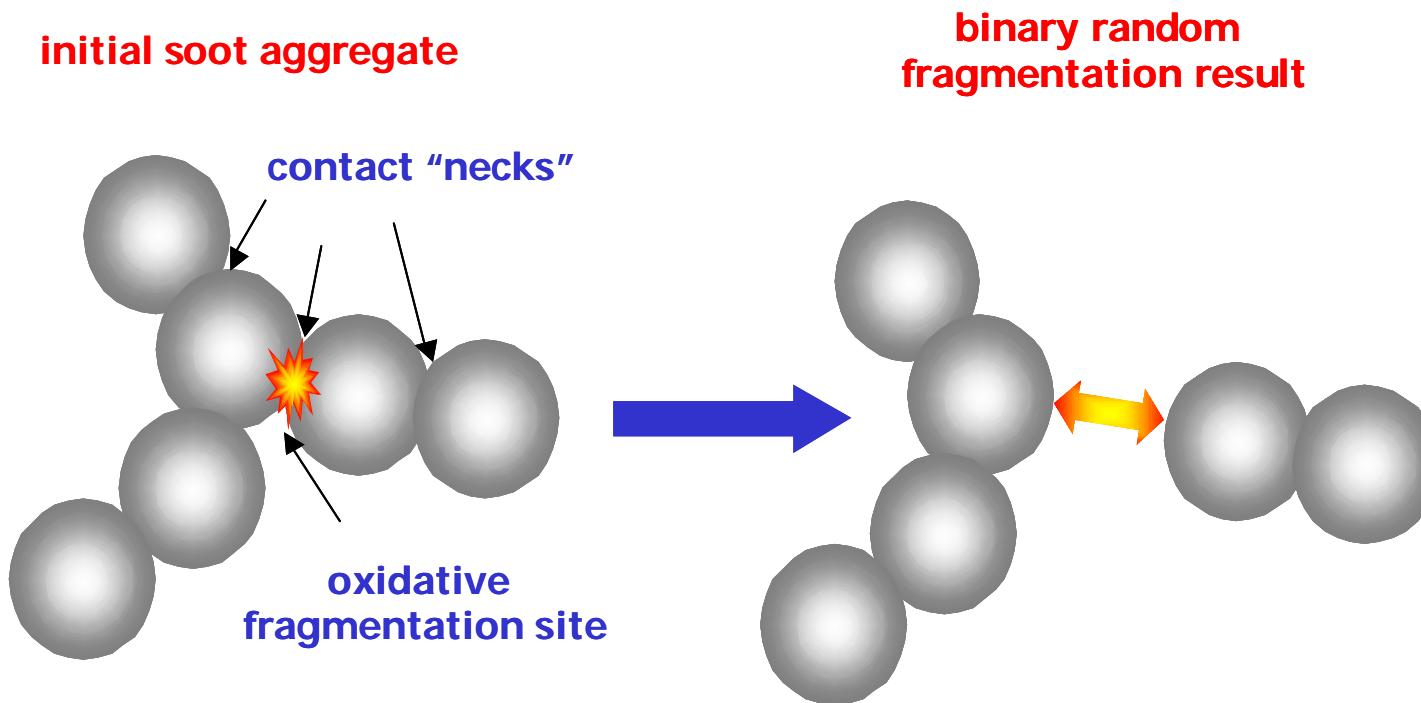
**Pump Unit Injector**



**Universal Lognormal Shape:**  
 $\sigma_g = 1.89 \pm 0.08$

cf. Harris & Maricq (2002) 1.7-1.8

## Steady state shape is determined from the ratio of oxidative fragmentation to coagulation rate



Continuous, binary random fragmentation process with size dependent rate:

$$S_i = Ai^b = Ai^{1/D_f}$$

In the large aggregate limit it can be shown that

$$\ln \sigma_g = \ln(6)/2(1+b)$$

For  $\sigma_g=1.89$ ,  $b = 0.42$  and  $D_f = 2.38$

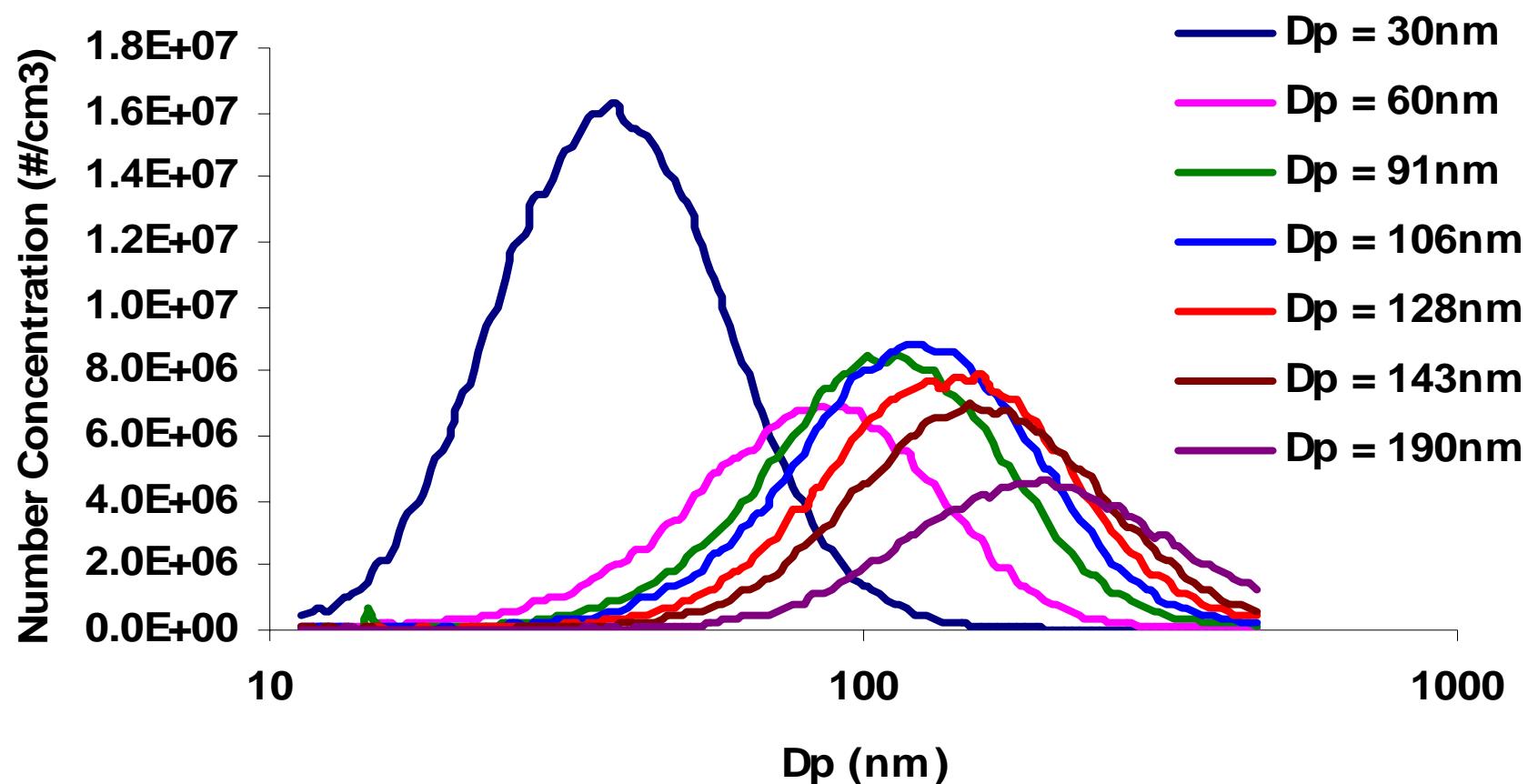
Kostoglou & Konstandopoulos (2003)

# CAST SOOT GENERATOR

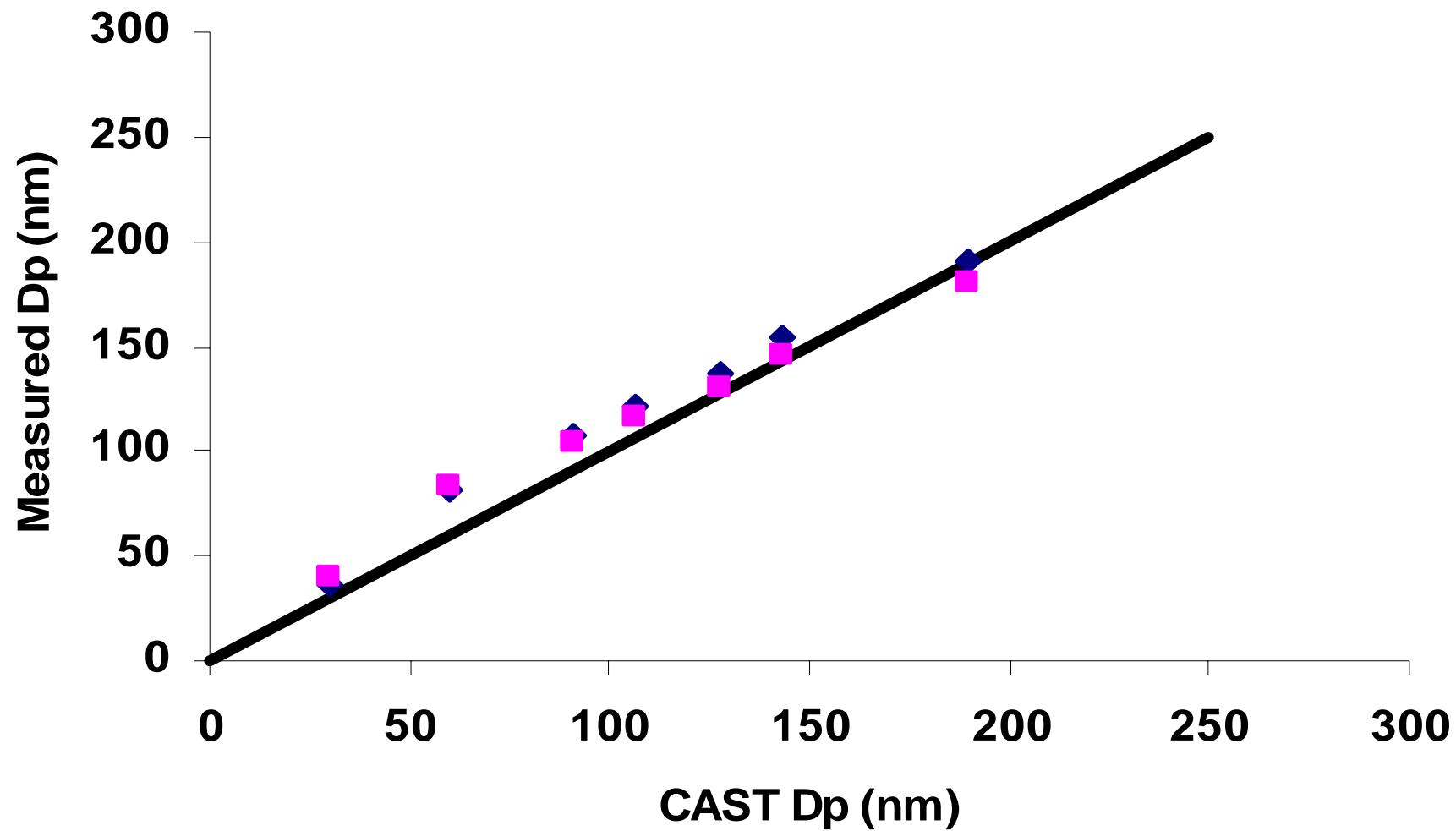
Provides Reference Soot Size Distributions



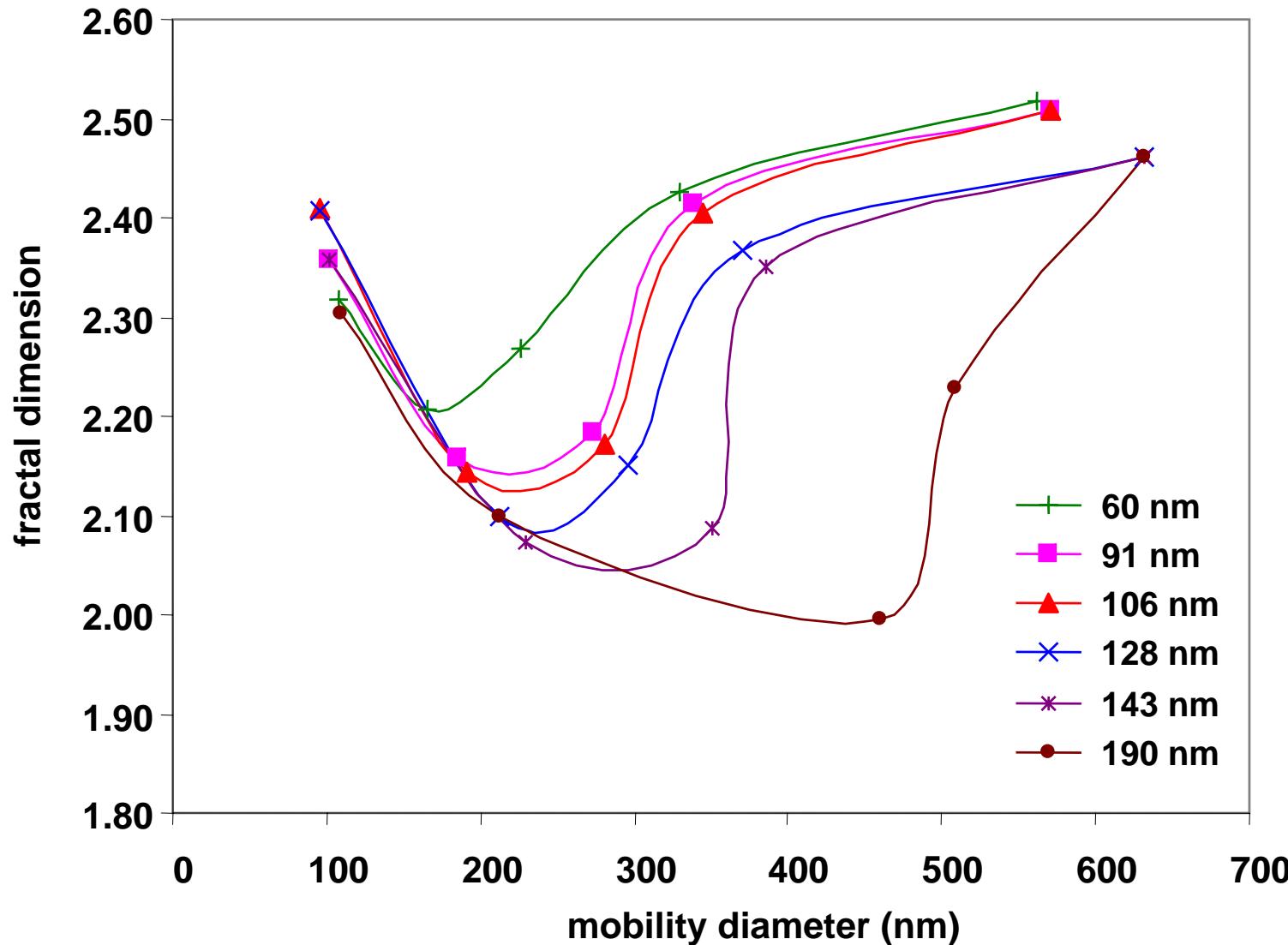
## SIZE DISTRIBUTIONS FROM CAST



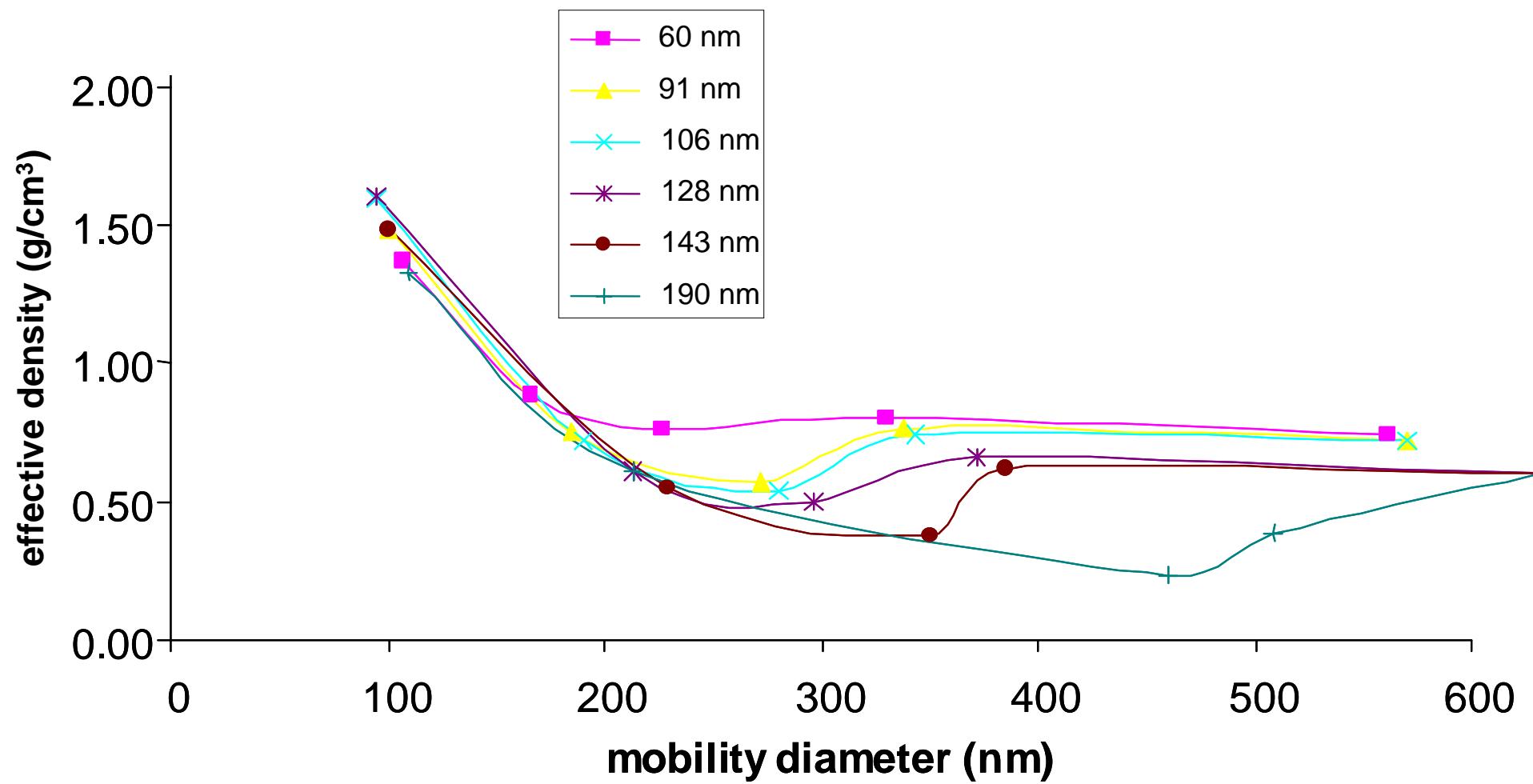
## CAST CALIBRATION WITH SMPS



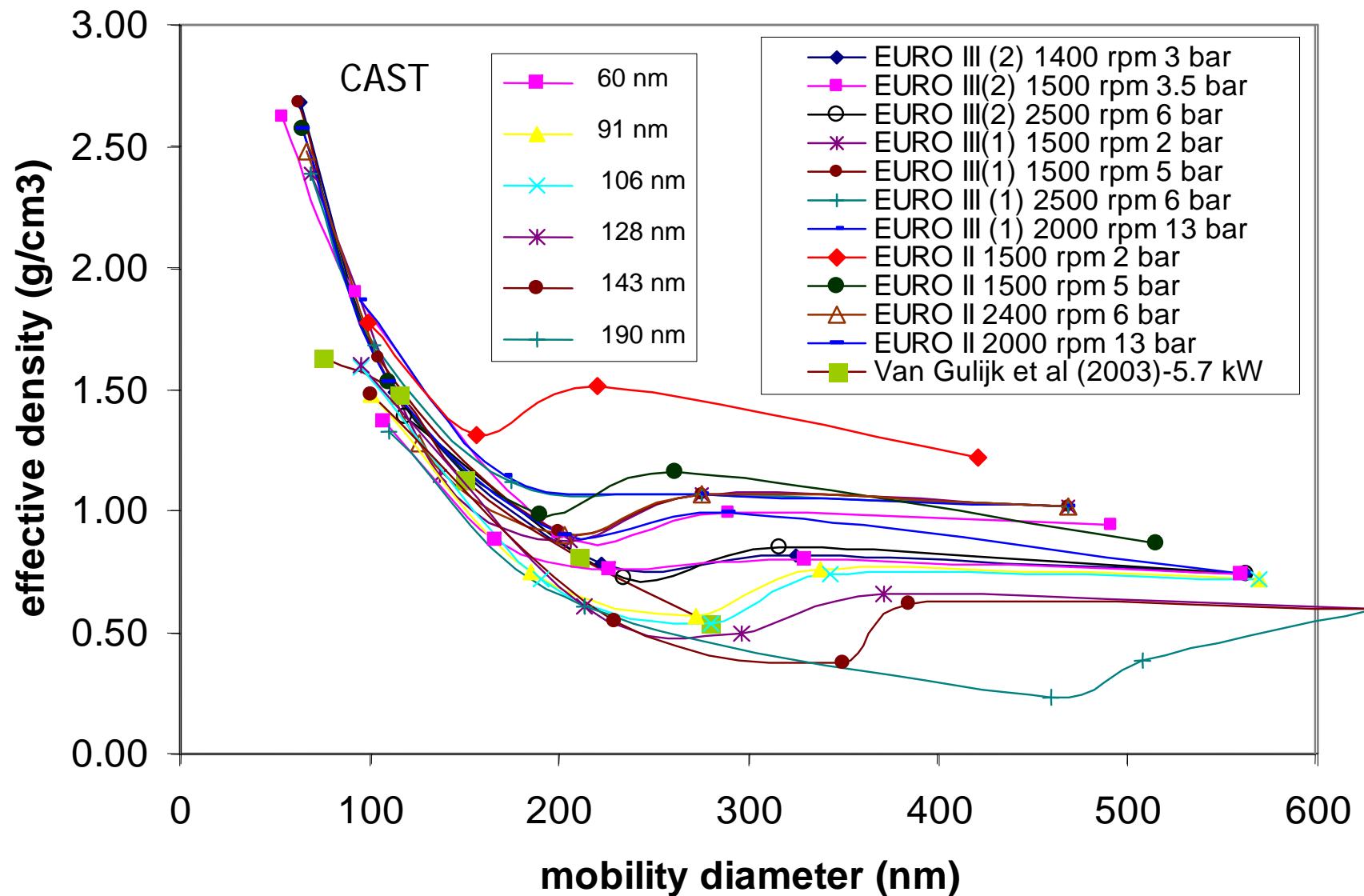
# CAST SOOT AGGREGATE FRACTAL DIMENSION



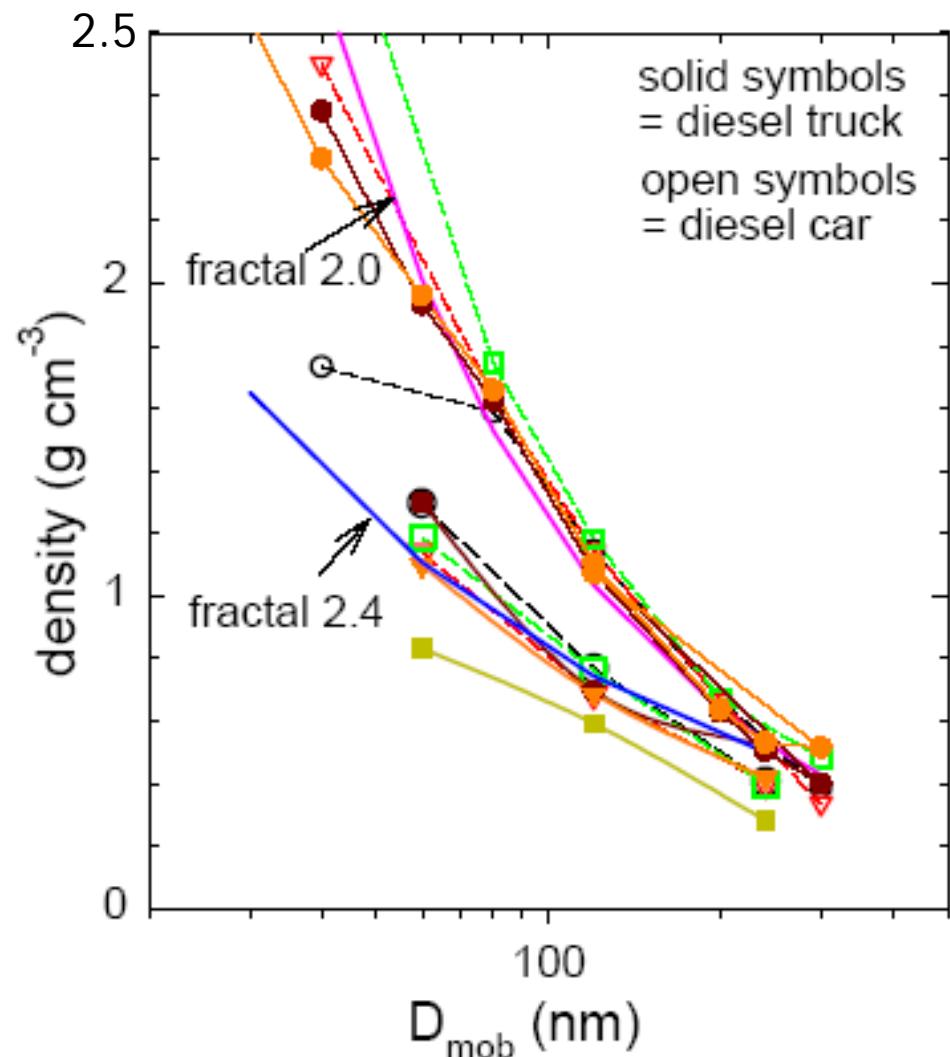
# CAST SOOT AGGREGATE EFFECTIVE DENSITY



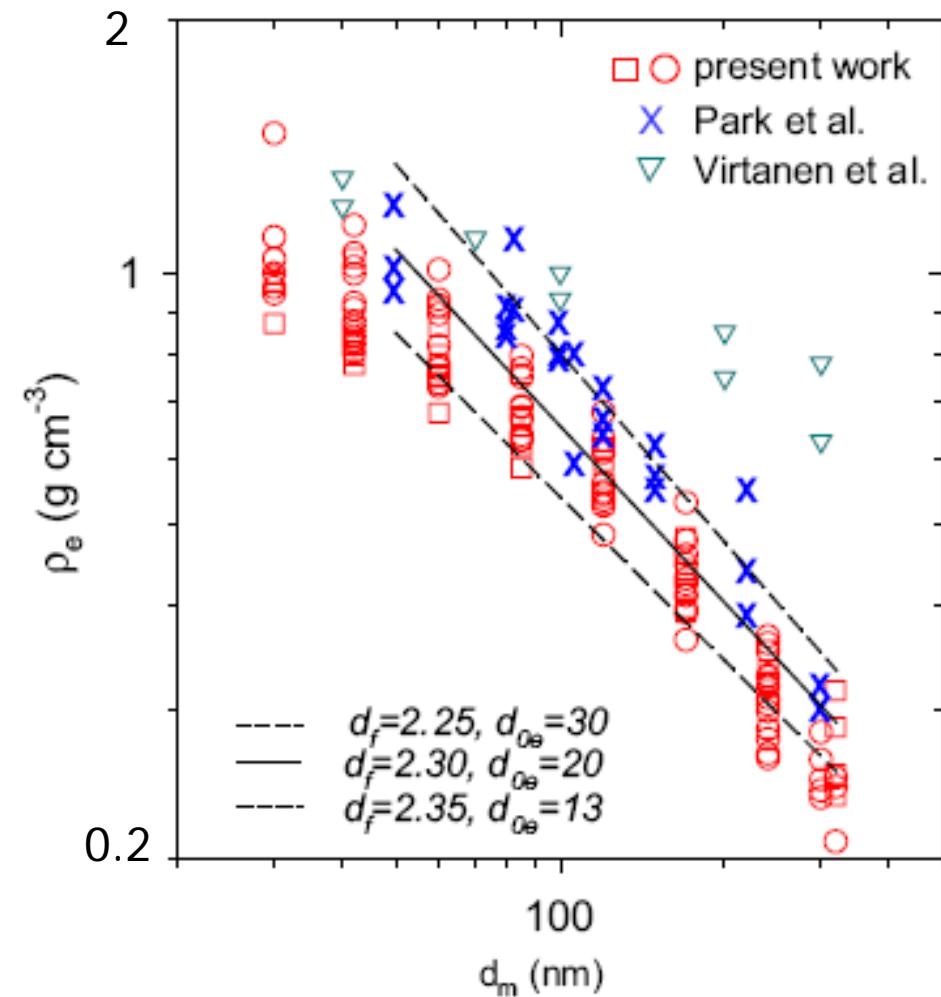
# SOOT AGGREGATE EFFECTIVE DENSITY: CAST & DIESEL



## OTHER STUDIES

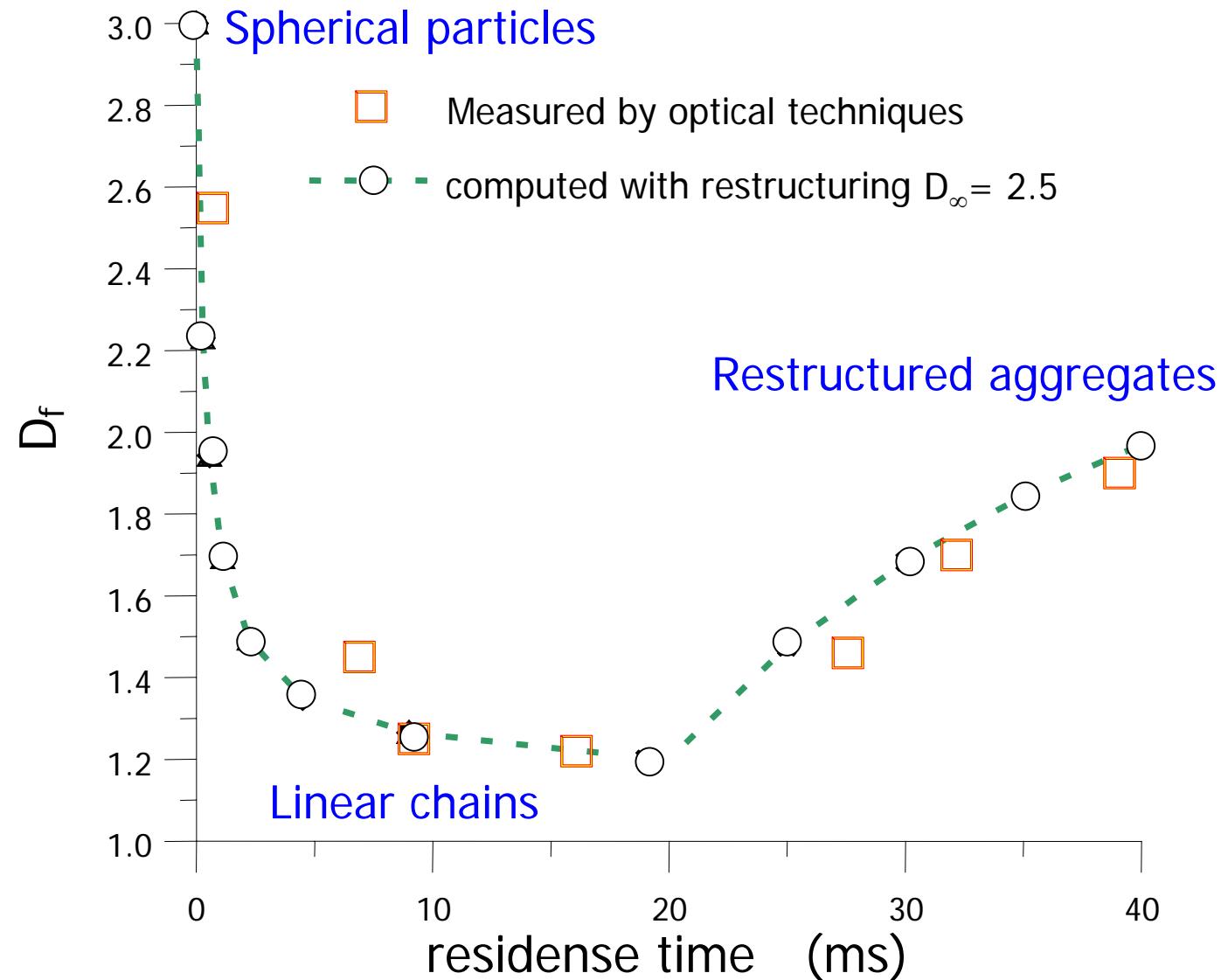


Maricq 2003 ELPI Workshop



Maricq & Xu (in press)

# SOOT FRACTAL DIMENSION EVOLUTION IN DIFFUSION FLAME



Di Stasio, Konstandopoulos & Kostoglou ( 2002)

## CONCLUSIONS

- Fractal dimension of soot from 3 diesel engines and a CAST burner changes non-monotonically with mobility diameter
- For diesel soot aggregates  $D_f$  decreases sharply from 3 down to  $\sim 1.8 - 1.9$  with aggregate size up to about 100 nm
- For larger than 100 nm aggregate sizes  $D_f$  increases up to  $\sim 2.4 - 2.5$
- An average  $D_f = 2.4$  for the entire aggregate population is consistent with the universal lognormal  $\sigma_g$  of  $1.89 \pm 0.08$  of many diesel size distributions based on population dynamics modelling of random oxidative fragmentation and coagulation
- Effective density exhibits a sharp decrease up to aggregate sizes about 200 nm and then a more gradual variation in agreement with the compaction shown by the increase of the  $D_f$  up to  $\sim 2.4 - 2.5$ .

## **ACKNOWLEDGMENTS**

- European Commission Quality of Life Project MAAPHRI and IST Project IMITEC for financial support
- Colleagues at the APT Lab: I. Papageorgiou, S. Skopa