Adhesion of Particles from Wood Combustion on Precipitation Surfaces

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1 Introduction

Particle properties play an important role in particle removal systems. An ideal operation of electrostatic precipitators (ESP) can only be achieved in a certain bandwidth of the electric conductivity of the particles [1]. Additionally, adhesion of particles is a key property in dust precipitation. It determines the minimum pressure impulse or the mechanical force needed to remove dust layers from fabric filters and ESP. Weak adhesion can cause re-entrainment in ESP, while high adhesion on the precipitation surface may lead to damages in ESP and fabric filters, potentially leading to the destruction of filter bags through conglutination.

For the operation of precipitators for wood combustion, it is essential to distinguish different combustion regimes [2] with dedicated particle categories [3] as follows:

- 1. Inorganic particles (salts) from almost-complete combustion
- 2. Soot from combustion with local lack of oxygen at high combustion temperatures
- 3. Condensable organic compounds (COC) formed at low combustion temperature.

It was shown in [3] that the electric conductivity of the particle categories varies by several orders of magnitude. The aim of the present work is to investigate and characterise the adhesion of particle layers from wood combustion. The adhesion of particles, especially in layers, is complex. Therefore, theoretical models to describe and calculate particle adhesion are scarce and it is hardly possible to reliably calculate adhesion of particle layers [4]. There are certain models for specific cases e.g. [5–7]. However, the number of factors is too high to adapt them in practice and hence experiments to characterise the properties are necessary and were conducted in the present work.

2 Method

Dust layers of one to two millimeters were collected in a laboratory scale tube ESP on bare steel and on electro polished steel. The dust samples were investigated during exposition to pressure impulses in a test channel of 100 mm x 16 mm x 18 mm in parallel to the dust layer. With this setup, the cleaning efficiency of the pressure impulse can be determined optically and quantified by the percentage of the cleared area as a function of the applied pressure impulse. According to the experimental results referred to in [1], the cleaning force needs to be increased by a factor of 10 to increase the cleaning efficiency from 50% to 98%. Consequently, it is possible to distinguish between different particle categories even in the case of relevant fluctuations and uncertainties.

Additional experiments with ultrasonic vibrations were made to determine adhesion according to acceleration forces. These experiments were carried out with an advanced ultrasonic dry-cleaning device, which finds the resonance of the test surface independently. Using this device, we measured about 1000 times the acceleration of gravity on our experimental surface.

3 Results

The results show that the pressure impulse needed to achieve a certain cleaning efficiency for the different particle layers varies by three orders of magnitude with increasing pressure impulse needed from soot to salt and to COC (Fig. 1).



Fig 1: Cleared area as a function of the applied pressure impulse, depending on the particle type on bare steel.

While the salt layer exhibits a medium adhesion, which can be characterised by a pressure for 50% cleaning efficiency according to area of app. 20 mbar, the required pressure impulse of app. 2 mbar is at the lower range of the experimental setup for soot. Consequently, soot is also expected to be potentially removed by re-entrainment in the ESP, which is not the case for layers of salts or COC. COC layers reveal high fluctuations at the upper boundary of the setup with an average of app. 200 mbar needed for 50% cleaning efficiency (Fig. 1).

By comparing the results of the cleaning of the three layers by ultrasonic vibration as shown in Table 1, salt shows the highest efficiency by acceleration which can be explained by its low porosity. Adhesion in salt layers is dominated by van der Waals forces. The porosity of soot is high as shown in Table 1. This causes a low density and an elastic behaviour. Consequently low detachment efficiencies due to acceleration forces are found for soot.

Liquid compounds increase the adhesion of COC. This leads to low efficiency in the ultrasonic vibration experiment for COC layers.

	Soot	Salt	COC
Detachment efficiency η at a $\approx 1000 \cdot g$	25 [a-%]	55 [m-%]	22 [m-%]
Density ρ _{Layer} [g/cm ³]	0.1	1.48	1.0
Porosity ε	94%	25%	17%
Physical properties	high elasticity & low density	low elasticity & high density	

Table 1: Detachment due to acceleration by ultrasonic vibrations depending on the particle type on electro polished steel. [a-%] = % of area, [m-%] = mass-%.

4 Conclusions

The presented investigation allow the following conclusions on adhesion:

- 1. Forces needed for dedusting precipitator surfaces depend on adhesion.
- Adhesion varies by more than three orders of magnitude depending on – the particle type and
 - the porosity of the particle layer.
- 3. For soot, the layer build-up in ESP is determined by its high electrical conductivity forming a layer with high porosity and weak adhesion.
- 4. Salt and Condensable Organic Compounds (COC) build a homogenous layer.
 For salts, van der Waals forces determine the adhesion.
 For COC, liquid compounds significantly increase adhesion.
- 5. Only minor influences on adhesion are found by
 - Surface roughness and
 - Flue gas humidity (determined by the water content of the fuel).

To use the presented results to dedust electrostatic precipitators or fabric filters, the following points have to be considered:

- The cleaning effect of aerodynamic drag depends on area (d²).
- The cleaning effect of acceleration depends on mass (d³) and porosity.
- Aerodynamic drag efficiency decreases from soot with high porosity to salt and to COC.
- Acceleration force is suited for salt removal, but limited for soot due to a high porosity and COC due to high adhesion.

5 References

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1. Introduction

- 2. Theory
- 3. Experimental Setup
- 4. Results
- 5. Conclusions



Process Steps in Particle Separation



 \rightarrow Forces needed for dedusting precipitator surfaces depend on adhesion.



*In case of particles including non-combustible ones, for soot only, the particle layer can be combusted

Particle Types





[Nussbaumer & Lauber, 2010] [Nussbaumer, 2003]



		Soot	Salt	COC
TOC	[m-%]	49	13	45
C/H	[mol/mol]	6.5	-	1.3
d _g	[nm]	200	65	80
C _m	[mg/m ³] @ 13% O ₂	70	20	30



Particle Property: Specific Dust Resistivity



*Dry: 5 vol.-% H_2O e.g. excess air ratio 3 & wood moisture content 5% *Wet: 20 vol.-% H_2O e.g. excess air ratio 1.2 & wood moisture content 50% *Ref: 13 vol.-% H_2O : excess air ratio 1.5 & wood moisture content around 30%



[Lauber & Nussbaumer, 2009] [3]: Parker, 1997

Layer Structures in ESP





acc.: [Blanchard et. al., 2002] [Lauber & Nussbaumer, 2009]



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Forces on Particle

	Effect		Force prop. to:
	Adhesion (Precipitation)		 van der Waals electrostatic d capillarity
	Detachment (Dedusting)	aerodynamic drag	 air current pressure impulse d²
		acceleration	 gravity mechanical impulse vibration centrifugal force
$\begin{array}{c} \text{mechanical impulse} \\ \hline \\ F_{Adhesion} = 0.063 \cdot d \cdot (1 + 0.009 \cdot \varphi) \\ \hline \\ \hline \\ F_{adhesion} = 0.063 \cdot d \cdot (1 + 0.009 \cdot \varphi) \\ \hline \\ \hline \\ \hline \\ F_{F_{G}} \\ \hline \\ F_{Pressure Impulse} \\ \hline \\ \hline \\ \hline \\ \hline \\ F_{Pressure Impulse} \\ \hline \\ $			



Adhesion vs. Detachment





Influence of Surface Roughness (e.g. in ESP) (Rabinovich equation)



 \rightarrow minor adhesion reduction due to polishing expected





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Experimental Setup: 1. Particle Sampling







Experimental Setup: 2. Pressure Impulse





Experimental Setup: 3. Ultrasonic Vibration



Analysis method:

salt and COC: weighting of removed particle agglomerates soot: optical determination of cleared area





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Dust Layer Build-up





[Lauber & Nussbaumer, 2009] [Friess & Yadigaroglu, 2002]

Results of Pressure Impulse



optical sub classification of COC :	Position in ESP	C/H-ratio
	[m]	[mol/mol]
coarse	0 – 0.3	1.56
fine	0.3 – 1	1.19



Results of Pressure Impulse

Influence of Surface: Bare vs. Electro Polished Steel



 \rightarrow no significant difference observed



Results of Ultrasonic Vibration

	Soot	Salt	COC
Efficiency η at a ≈ 1000⋅g	25 [a-%]	55 [m-%]	22 [m-%]
			DP
	(soot: black)	(salt: dark grey)	(COC: light brown)
Density ρ_{Layer} [g/cm ³]	0.1	1.48	1.0
Porosity ε	94%	25%	17%
Physical properties	high elasticity & low density	low elasticity & high density	





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5. Conclusions



1. Conclusions on Adhesion

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 - Flue gas humidity (determined by the water content of the fuel).



2. Conclusions on Removal Methods

The cleaning effect of aerodynamic drag depends on area (d²). The cleaning effect of acceleration depends on mass (d³) and porosity.

Consequences:

Aerodynamic drag efficiency decreases from soot (high porosity) to salt and COC (liquids).

Acceleration force is

- suited for salt removal
- but limited for soot (high porosity) and COC (high adhesion)





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