

Background

The growth of air traffic has generated environmental concern since engine emissions can impact air quality around airports as well as general atmospheric chemistry and climate. An accurate assessment requires that the physical properties, e.g. number concentration, size, mass density, of the PM within the exhaust as it exits the engine, along with its evolution in the aging plumes, be understood and well characterized.

The SAE E31 committee is currently working to develop an ARP (Aerospace Recommended Practice) for gas turbine exhaust nvPM (non-volatile Particulate Matter) number and mass measurements. MS&T has assembled a reference system for this task, including both sampling train and instrumentation.

Honeywell Test Campaign

- July/August 2014
- Intercomparison of the AIR6241 compliant North American mobile reference system operated by MS&T and the Honeywell nvPM System.
- Honeywell turbofan propulsion engine in the 29 – 33 kN thrust range.
- Honeywell San Tan Remote Facility – Phoenix Arizona

Objectives

- Inter-compare HON system and North American nvPM Reference system
- Compare nvPM emissions sampled from mixed flow and core flow configurations
- **Compare nvPM emissions from tests conducted during different times of the day to investigate the impact of variation in ambient temperature**

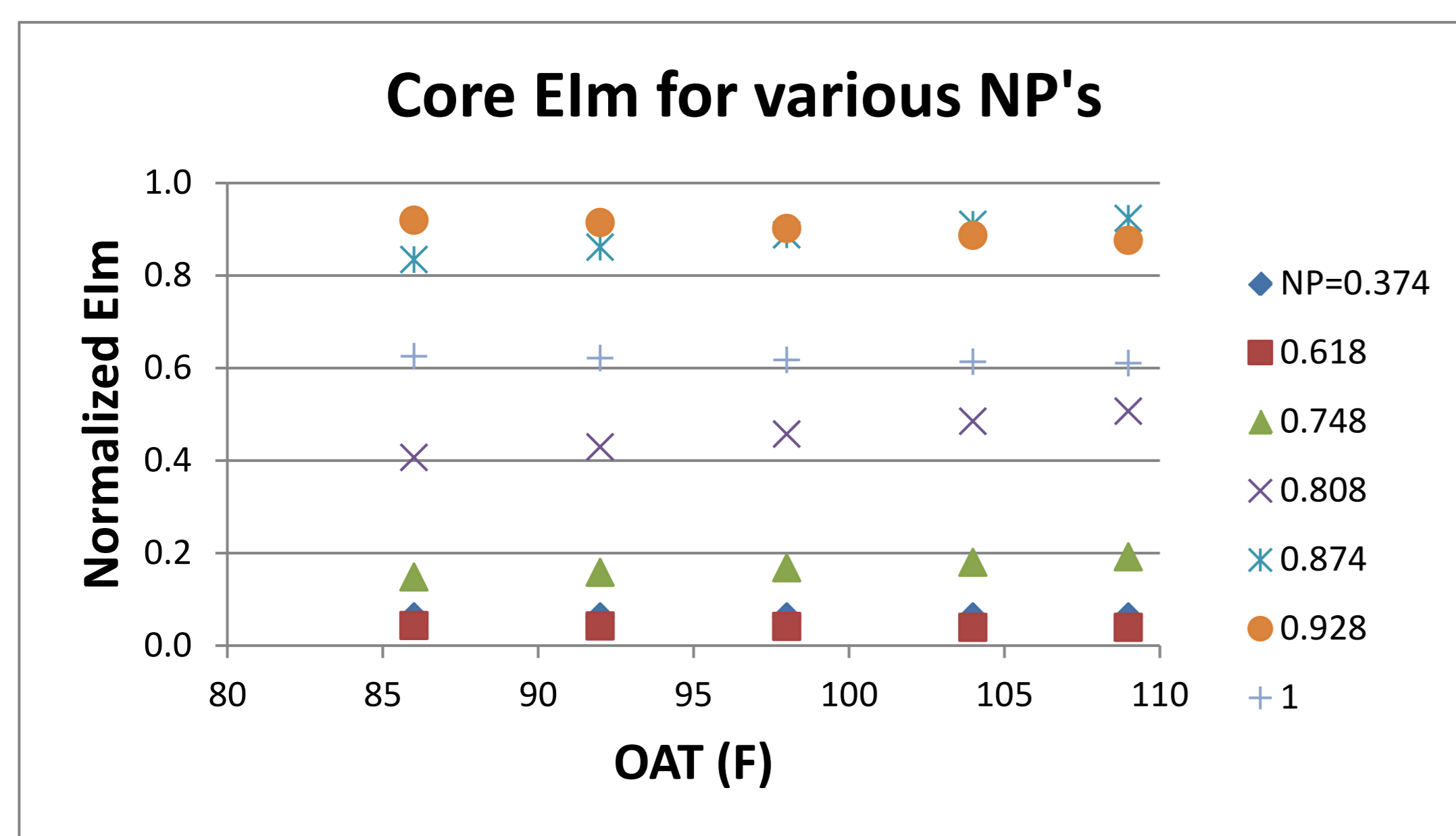
Instrumentation

- Number: AVL Particle Counter (APC)
- Mass: AVL Micro Soot Sensor (MSS)
- DMS500 Fast particle size spectrometer

Parameters

Elm – Mass based emission index
 ElmC – Elm corrected for line loss.
 GMD – Geometric Mean Diameter
 GSD – Geometric Standard Deviation
 MMD – Mass Mean Diameter
 EIn – Number based emission index.
 EInC – EIn corrected for line loss.

Analysis Elm, EIn, GMD, GSD



- OAT denotes outside air temperature.
- NP is a normalized surrogate for engine power.
- Uncertainty weighted linear fit, for each NP.
- Slope, intercept, δ slope, δ intercept
- Change in aerosol parameter over $\Delta T = 23$ F
 $-\text{slope} * \Delta T$
- Uncertainty in that change
 $-\delta \text{slope} * \Delta T$
- Ratio = $\delta \text{slope} / \text{slope}$
 $-\leq 1 \rightarrow$ Change in Elm is statistically significant

	Slope Matrix						
Parameter ↓ / NP →	0.374	0.618	0.748	0.808	0.874	0.928	1.000
Elm	0.013	-0.113	1.121	2.768	2.286	-1.219	-0.378
ElmC	0.013	-0.113	1.121	2.768	2.286	-1.219	-0.378
GMD	-0.021	-0.003	0.022	0.074	0.042	-0.084	-0.094
GSD	0.001	0.000	0.000	0.000	0.000	0.000	0.000
MMD	0.281	0.281	0.281	0.281	0.281	0.281	0.281
EIn	-0.003	-0.001	0.001	0.006	0.000	0.007	0.003
EInC	-0.003	-0.001	0.002	0.007	0.000	0.009	0.005

	δ slope/slope Matrix						
Parameter ↓ / NP →	0.374	0.618	0.748	0.808	0.874	0.928	1.000
Elm	11.32	0.38	0.40	0.30	0.20	0.19	0.41
ElmC	11.32	0.38	0.40	0.30	0.20	0.19	0.41
GMD	0.74	1.82	0.70	0.37	0.24	0.09	0.10
GSD	0.94	0.92	3.61	0.24	2.78	2.11	0.43
MMD	0.28	0.28	0.28	0.28	0.28	0.28	0.28
EIn	1.34	0.16	1.15	0.33	1.21	0.05	0.04
EInC	1.65	0.22	1.02	0.34	1.61	0.05	0.05

	% change Matrix, $\Delta OAT = 23$ F				100*23*slope/average			
Parameter ↓ / NP →	0.374	0.618	0.748	0.808	0.874	0.928	1.000	
Elm	1	-10	25	23	10	-5	-2	
ElmC	1	-10	25	23	10	-5	-2	
GMD	-2	0	1	4	2	-4	-4	
GSD	2	0	0	0	0	0	1	
MMD	11	10	8	7	6	5	5	
EIn	-7	-4	3	9	0	11	11	
EInC	-6	-3	4	8	0	11	10	

Results for core flow

- $\delta \text{slope} / \text{slope}$ usually ≤ 1
- There is statistically significant temp effect, up to 25% for a 23F change in OAT.
- The effect is stronger at high power.
- Where $\delta \text{slope} / \text{slope} > 1$
 –Parameter vs OAT is pretty flat
 –The %change is small.

Acknowledgment

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