

A Methodology to Relate Black Carbon Particle Number and Mass Emissions from Various Combustion Sources

Roger Teoh¹, Marc E.J. Stettler¹, Arnab Majumdar¹ and Ulrich Schumann²

*Corresponding author: rt415@ic.ac.uk

¹Centre for Transport Studies, Department of Civil and Environmental Engineering, Imperial College London, London, SW7 2AZ, UK.

²Deutsches Zentrum für Luft- und Raumfahrt, Institute of Atmospheric Physics, 82234 Oberpfaffenhofen, Germany

1. Introduction

- Black Carbon (BC) Particle Number (PN) emissions from the transport sector influences health and climate, yet its impact remain highly uncertain.
- Health Effects:** Ultrafine particles have a higher probability of being deposited into the respiratory system, and translocated towards the circulatory system and internal organs.
- Climate Effects:** BC PN emissions from aircraft acts as a condensation nuclei for contrail formation, where the initial contrail properties are strongly correlated to the number of emitted aircraft BC particle per kg of fuel burned (EI_n in kg^{-1}) (Fig. 1) [1].
- Existing BC EI_n models for aviation emissions assumes that BC particle morphologies remain constant irrespective of engine thrust settings.
- Aims & Objectives:**
 - Develop a new model to estimate BC PN emissions from mass using the theory of fractal aggregates.
 - Validate the new model using BC measurements from three different emission sources
 - Perform an uncertainty and sensitivity analysis to understand the accuracy and uncertainty bounds of the outputs of the newly developed model.

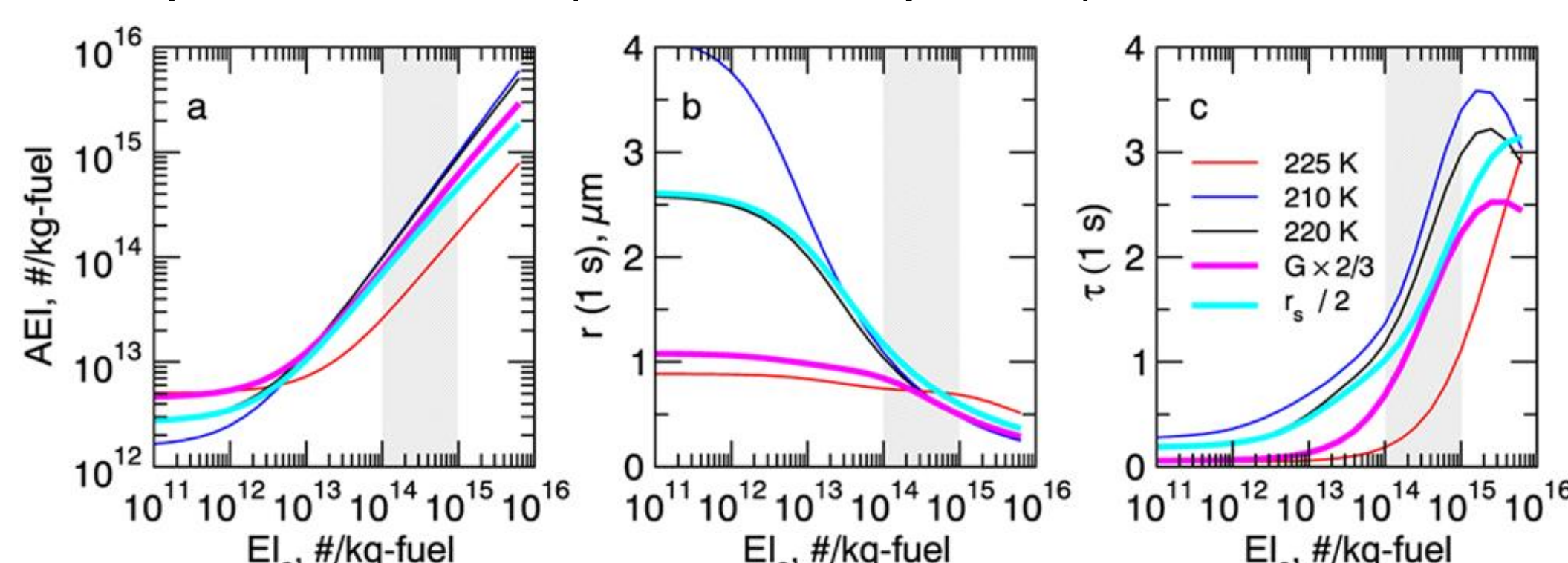


Fig. 1: Changes in contrail properties versus BC EI_n in a young contrail. These contrail properties are reported at a plume age of 1-second. (Source: [1])

2. Theory – Development of a new BC N or EI_n Predictive Model

Nomenclature

m	Mass of one BC aggregates	n_{pp}	Number of primary particles in an aggregate
d_m	Aggregate Mobility Diameter	d_{pp}	Primary Particle Diameter
ρ_0	BC Material density	k_a & D_α	Scaling prefactor & projected area exponent
D_{fm}	Aggregate mass-mobility exponent	k_{TEM} & D_{TEM}	TEM prefactor-exponent coefficient pairs
GMD	Geometric Mean Diameter	$n(d_m)$	No. of aggregates for a given mobility diameter range
GSD	Geometric Standard Deviation	M & N	Total mass and number of BC aggregates

- In a free molecular regime, $n_{pp} = k_a \left(\frac{d_m}{d_{pp}}\right)^{2D_\alpha}$ or $n_{pp} = \left(\frac{d_m}{d_{pp}}\right)^{D_{fm}}$ [2],
 - where constant values of $k_a = 0.998$ and $D_\alpha = 1.069$ can be used for aggregates formed of polydisperse primary particles, irrespective of the state of sintering [3].

- Total mass of aggregates for a given Particle Size Distribution (PSD):

$$n_{pp} = k_a \left(\frac{d_m}{d_{pp}}\right)^{2D_\alpha} \quad d_{pp} = k_{TEM} \times d_m^{D_{TEM}} \quad [4]$$

$$m = n_{pp} \rho_0 \left(\frac{\pi}{6}\right) d_{pp}^3 \quad n(d_m) = N \times p(d_m)$$

$$M = \int_0^\infty m(d_m) n(d_m) d \ln d_m \quad \rightarrow \quad M = N k_a \rho_0 \left(\frac{\pi}{6}\right) (k_{TEM})^{3-2D_\alpha} \int_0^\infty d_m^\phi p(d_m) d \ln d_m$$

- Resolve the remaining integral (ϕ^{th} moment of a log-normal distribution) & rearrange for N :

$$N = \frac{M}{k_a \rho_0 \left(\frac{\pi}{6}\right) (k_{TEM})^{3-2D_\alpha} \text{GMD}^\phi \exp\left(\frac{\phi^2 \ln(\text{GSD})^2}{2}\right)}, \quad \text{where } \phi = 3D_{TEM} + (1 - D_{TEM})2D_\alpha.$$

- BC aggregate morphology and PSD, such as the GMD, GSD and D_{fm} are dependent on engine operating mode & combustion conditions.
- The new Fractal Aggregates (FA) model relates BC mass, number and PSD in one equation.

3. Data & Methodology

- The FA Model is validated with data from (i) An internal combustion engine [5], (ii) An inverted burner [6], and (iii) Two aircraft gas turbine engines at ground and cruise conditions [7], [8].
- An uncertainty analysis for the FA model is performed using the Monte Carlo 1000-member ensembles, while a global sensitivity analysis is accomplished using the Sobol' Method [9].

4. Model Validation

Internal Combustion Engine & Inverted Burner

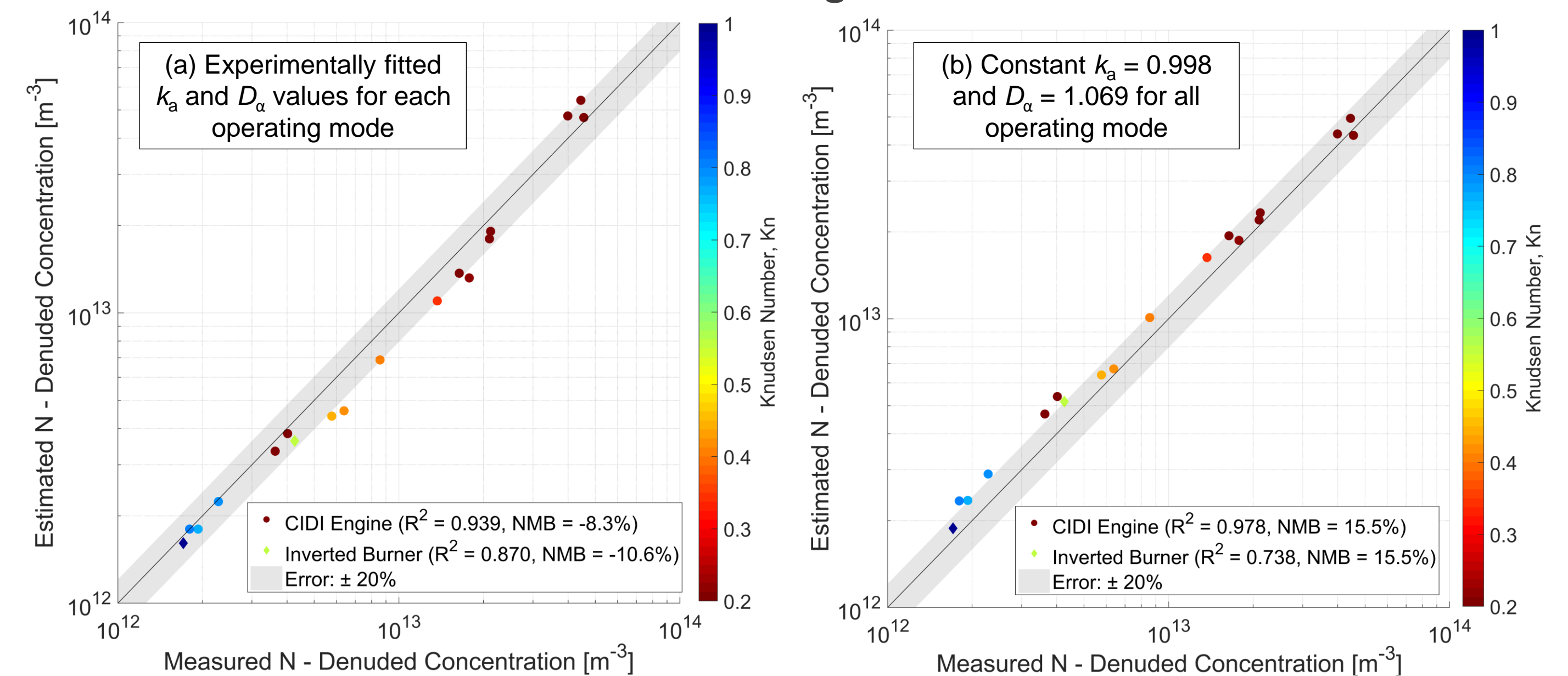


Fig. 2: Validation of the FA Model with data from an internal combustion engine & inverted burner

- For two different sets of k_a and D_α values, the difference in the FA model outputs (estimated N) is within $\pm 20\%$ of the measured N . Hence, constant values of $k_a = 0.998$ and $D_\alpha = 1.069$ can be used when specific k_a and D_α data for a given operating condition is not available.

Aircraft Gas Turbine Engines at Ground and Cruise Conditions

For aircraft emissions, we assume $k_a = 1$ & $D_\alpha = \frac{1}{2} D_{fm}$ [Recall: $n_{pp} = k_a \left(\frac{d_m}{d_{pp}}\right)^{2D_\alpha}$ or $n_{pp} = \left(\frac{d_m}{d_{pp}}\right)^{D_{fm}}$]

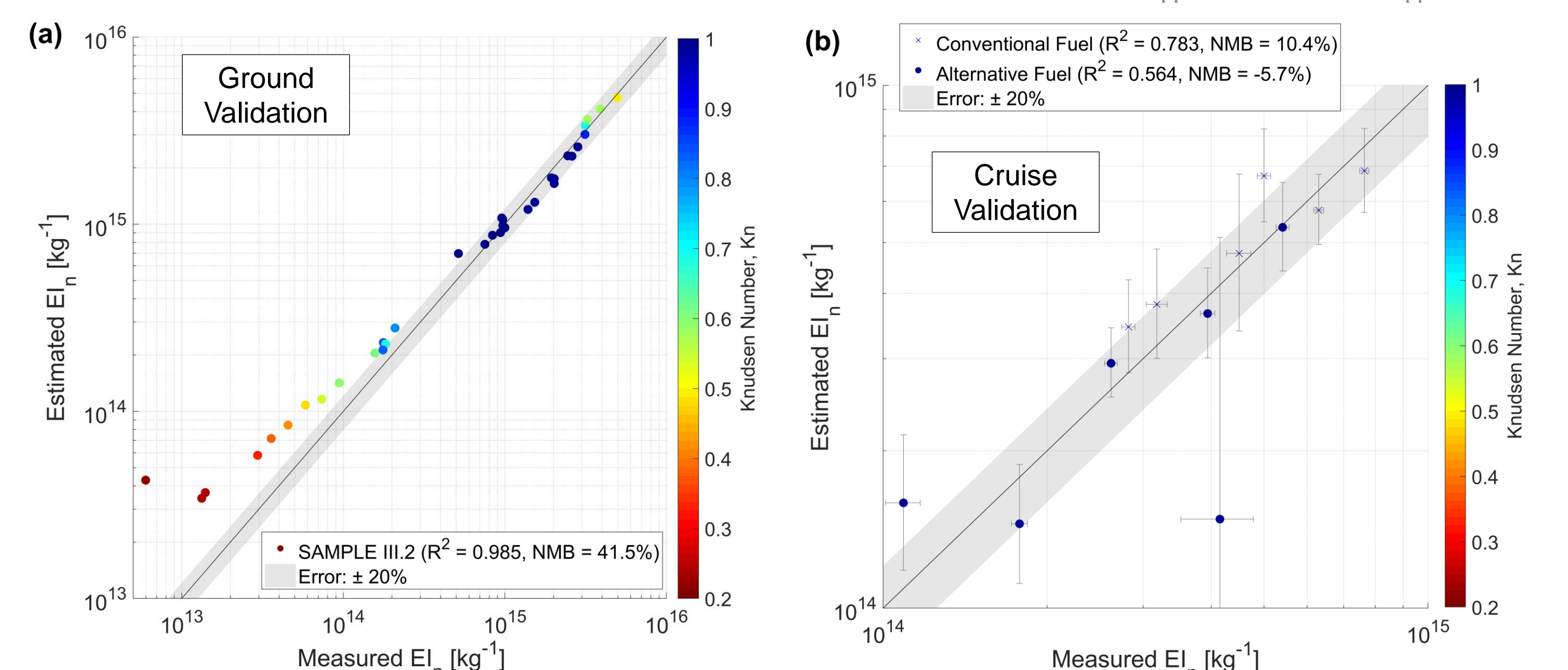


Fig. 3: FA Model validation with aircraft gas turbine engine data at (a) ground and (b) cruise conditions

- For ground validation (Fig. 3a), a systematic overestimation of EI_n is observed at higher thrust settings (data points with lower Kn) as BC aggregates are formed in the continuum regime.

5. Uncertainty & Sensitivity Analysis

- Due to the non-linearity of the FA model, the uncertainty of the estimated N or EI_n is asymmetrically distributed (-37% , $+55\%$) at 1.96σ (Fig. 4a).
- Sensitivity analysis (Fig. 4b) identified that the uncertainties in GSD contribute to the largest sensitivity in the FA model output, followed by inputs of M , D_{fm} and GMD.
- A prioritisation can be recommended for future research to measure these critical parameters more accurately to reduce the uncertainty bounds of the FA model outputs.

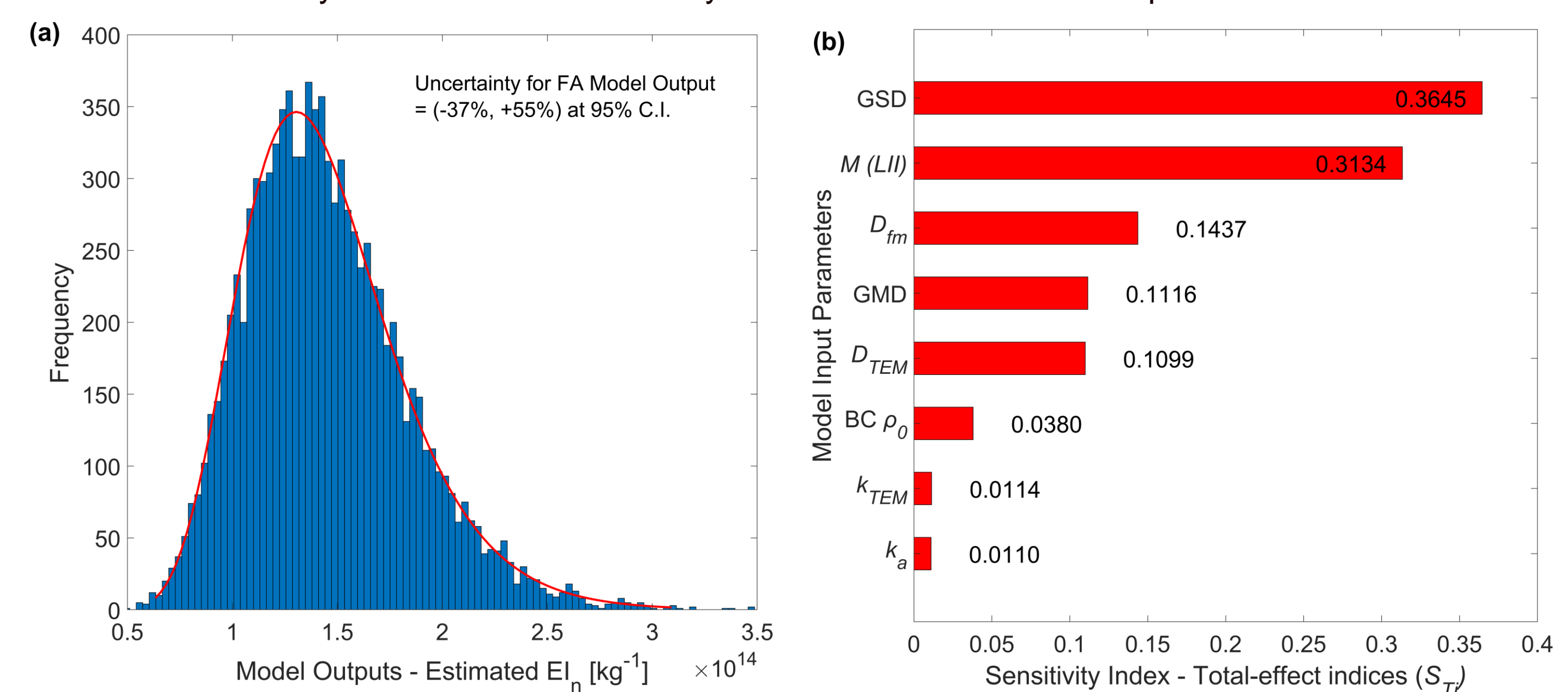
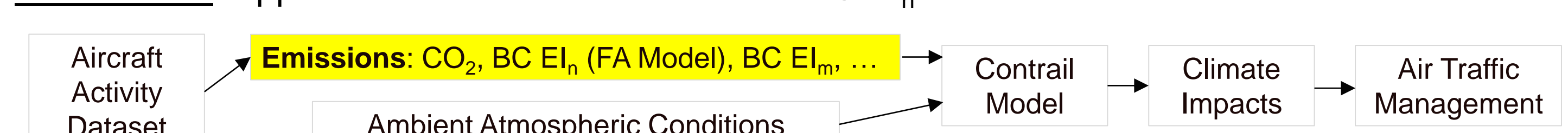


Fig. 4: (a) Uncertainty & (b) Sensitivity Analysis for the FA model outputs (Estimated N or EI_n)

Summary & Future Work

- A new methodology to relate BC Particle Number and Mass emissions is developed based on the theory of fractal aggregates, and validated with three different BC emission sources.
- Large uncertainties remain; GMD, GSD, M & D_{fm} inputs are identified as important parameters.

- Future Work:** Application of FA Model to estimate BC EI_n for Aviation Emissions



References

- [1] Kärcher, B. (2016) The importance of contrail ice formation for mitigating the climate impact of aviation. *Journal of Geophysical Research: Atmospheres*, 121 (7), 3497-3505.
 [2] Sorensen, C.M., 2011. The mobility of fractal aggregates: a review. *Aerosol Science and Technology*, 45(7), pp.765-779
 [3] Eggersdorfer et al. (2012) Aggregate morphology evolution by sintering: number and diameter of primary particles. *Journal of aerosol science*, 46, pp.7-19.
 [4] Dastanpour, R. & Rogak, S. N. (2014) Observations of a correlation between primary particle and aggregate size for soot particles. *AST*, 48 (10), 1043-1049.
 [5] Graves et al. (2015) Characterization of particulate matter morphology and volatility from a compression-ignition natural-gas direct-injection engine. *AST*, 49(8), pp.589-598.
 [6] Dastanpour et al. (2017) Variation of the optical properties of soot as a function of particle mass. *Carbon*, 124, pp.201-211.
 [7] Boies et al. (2015) Particle emission characteristics of a gas turbine with a double annular combustor. *AST*, 49 (9), 842-855.
 [8] Moore et al. (2017) Biofuel blending reduces particle emissions from aircraft engines at cruise conditions. *Nature*, 543 (7645), 411-415.
 [9] Saltelli et al. (2008) *Global sensitivity analysis: the primer*, John Wiley & Sons
 [10] Lobo et al. (2015) PM emissions measurements of in-service commercial aircraft engines during the Delta-Atlanta Hartsfield Study. *Atmospheric Environment*, 104, pp.237-245.