

# Effective Density and IPSD Measurements of solid PM from a Lean and Stoichiometric GDI Engine Operating on Ethanol Blends

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# Outline

- Introduction
- Effective Density
- Size Distributions
- Solid Particle Number and MSS Black Carbon Mass
- Integrated Particle Size Distribution (IPSD) Mass vs Black Carbon Mass
- Summary

# Introduction

- Gasoline direct injection (GDI) engines are being widely adapted for light-duty vehicles
  - Increased power output
  - Higher efficiency
  - Reduced CO<sub>2</sub> emissions
- But GDI engines produce higher levels of PM and PN, especially lean burn engines
- Lean burn GDI
  - **Higher efficiency – approaching Diesel**
  - More difficult to control NOx emissions
  - May have higher PM, PN emissions
  - Limited applications in Japan , Europe
  - Not used in US – stoichiometric burn only

# Engine and fuels

<b>Table 1. Engine specifications.</b>	
Model Number	BMW N43B20
Displacement (cc)	1995
Bore x Stroke (mm)	84 x 90
Compression Ratio	12:1
Rated Power (kW)	125 @ 6700 rpm
Rated Torque (Nm)	210 @ 4250 rpm
Induction	Naturally Aspirated
Injection	Central Spray Guided Piezo
Max Rail Pressure (bar)	200

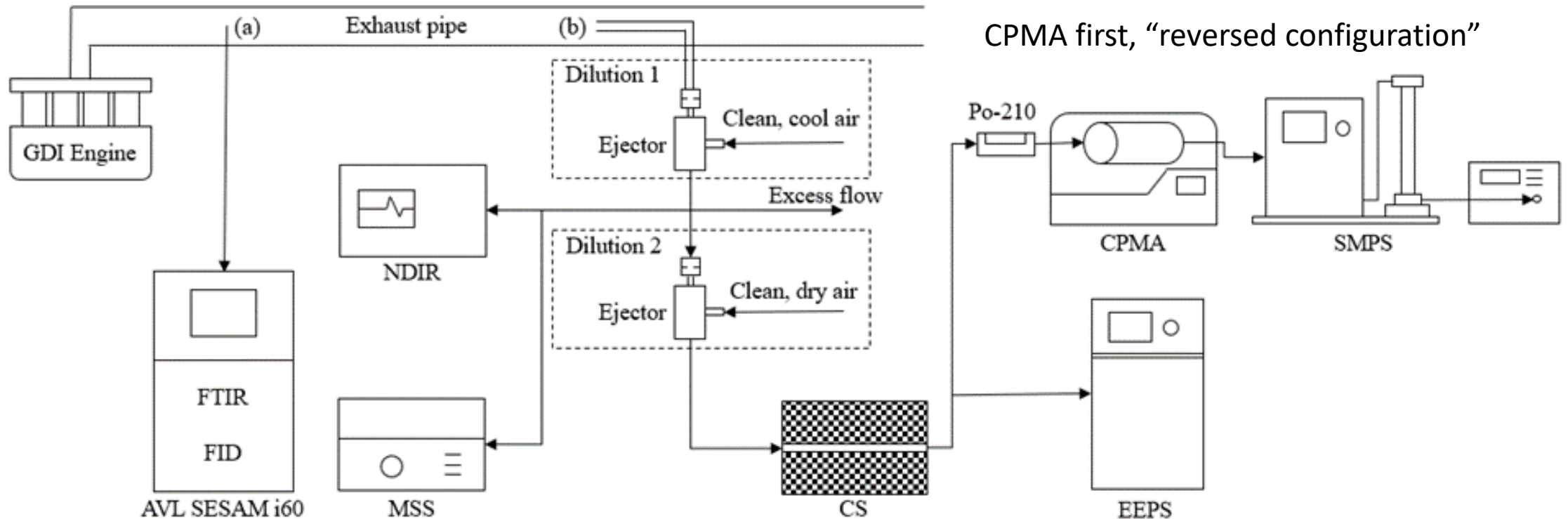
<b>Table 2. Fuel specifications.</b>				
Fuel	Aromatics (%)	T90 (°C)	EtOH (%)	RON/MON (AKI)
E10 (Baseline)	27	162	9.9	96.2/85.4 (90.8)
E30	21	-	30	-
E50	15	-	50	-

<b>Table 3. Engine testing conditions: S=stoichiometric; LH=Lean homogeneous; LS=lean stratified</b>			
Speed (RPM)	BMEP (bar)	Mode	Fuel-air equivalence ratio
2000	7	S	1
2000	7	LH	0.69
2000	4	LS	0.65

# Instruments

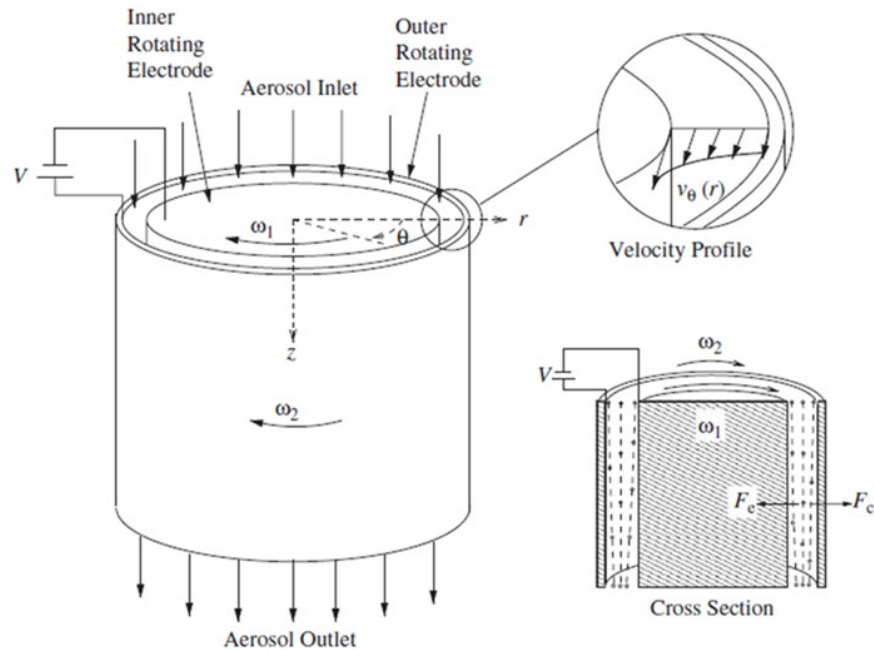
- Particle size distributions
  - TSI EEPS (5.6 to 560 nm) using soot inversion matrix
  - Catalytic stripper to remove semi-volatile particles
- Black carbon – AVL Micro Soot Sensor
- Effective density –
  - Combustion CPMA – TSI SMPS so called “reversed” method much faster
  - TSI DMA – CPMA – CPC – traditional method validation check
- Solid particle mass and number by integrated particle size distribution (IPSD) method

# Experimental Setup



# Effective density and IPSD mass

- CPMA mass,  $m$ , and DMA mobility diameter,  $d_m$ , used to find effective density.
- EEPS size distribution and effective density distribution used to find integrated size distribution (IPSD) mass



$$mr\omega^2 = qE = \frac{N_q eV}{r \ln\left(\frac{r_o}{r_i}\right)}$$

$$\frac{m}{N_q} = \frac{eV}{r^2 \omega^2 \ln\left(\frac{r_o}{r_i}\right)}$$

$$m = kd_m^{Dmm}$$

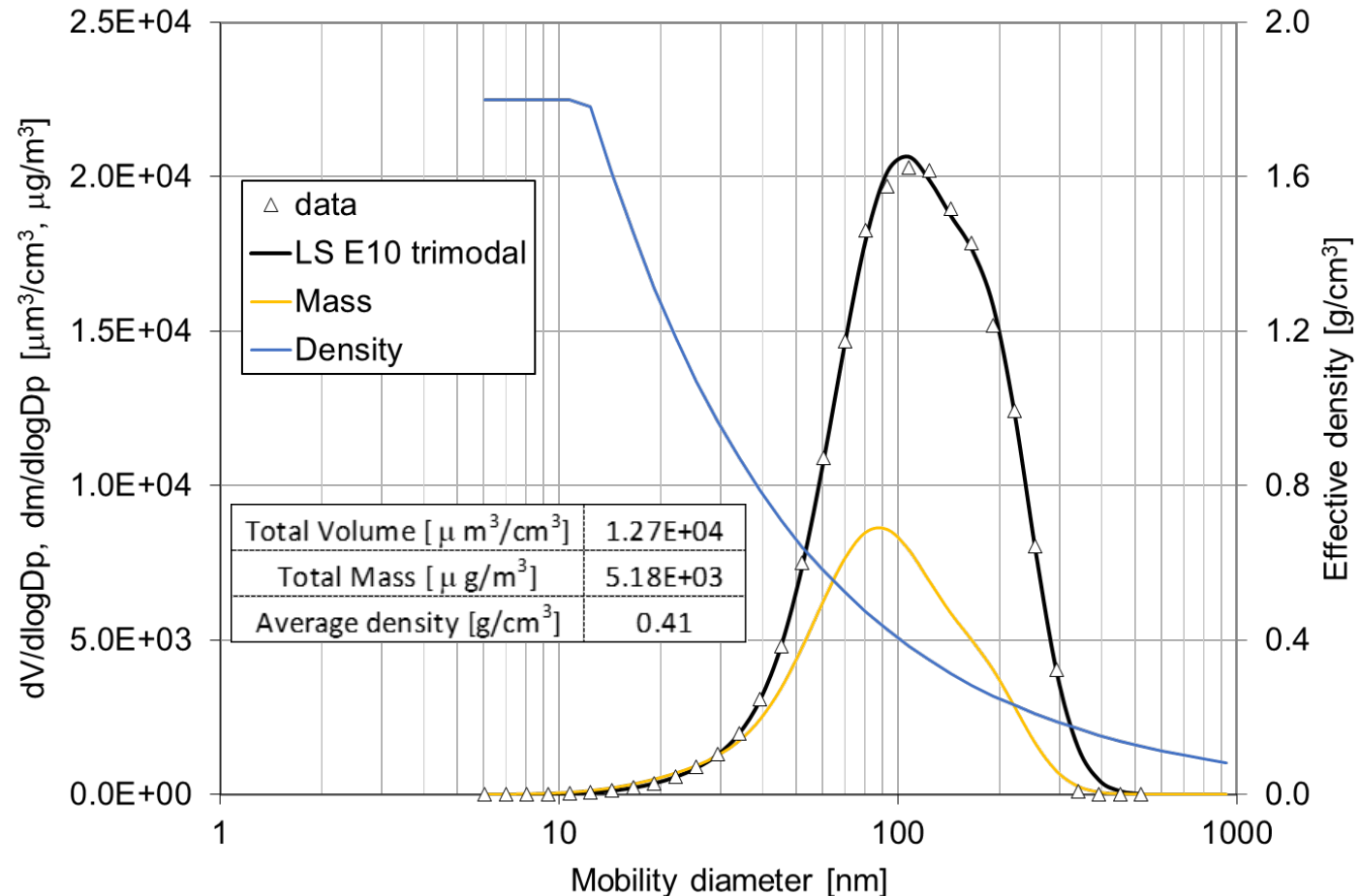
$$\rho_{eff} = \frac{m}{\pi \frac{d_m^3}{6}} = \frac{6k}{\pi} d_m^{(Dmm-3)}$$

$$\frac{dV(d_m)}{d\text{Log}(d_m)} = \frac{dN(d_m)}{d\text{Log}(d_m)} \frac{\pi(d_m)^3}{6}$$

$$\text{IPSD}(\text{mass}) = \int \rho_{eff}(d_m) \frac{dV(d_m)}{d\text{Log}(d_m)} d\text{Log}(d_m)$$

Adapted from Olfert, et al., JAS 37 (2006) 1840-1852

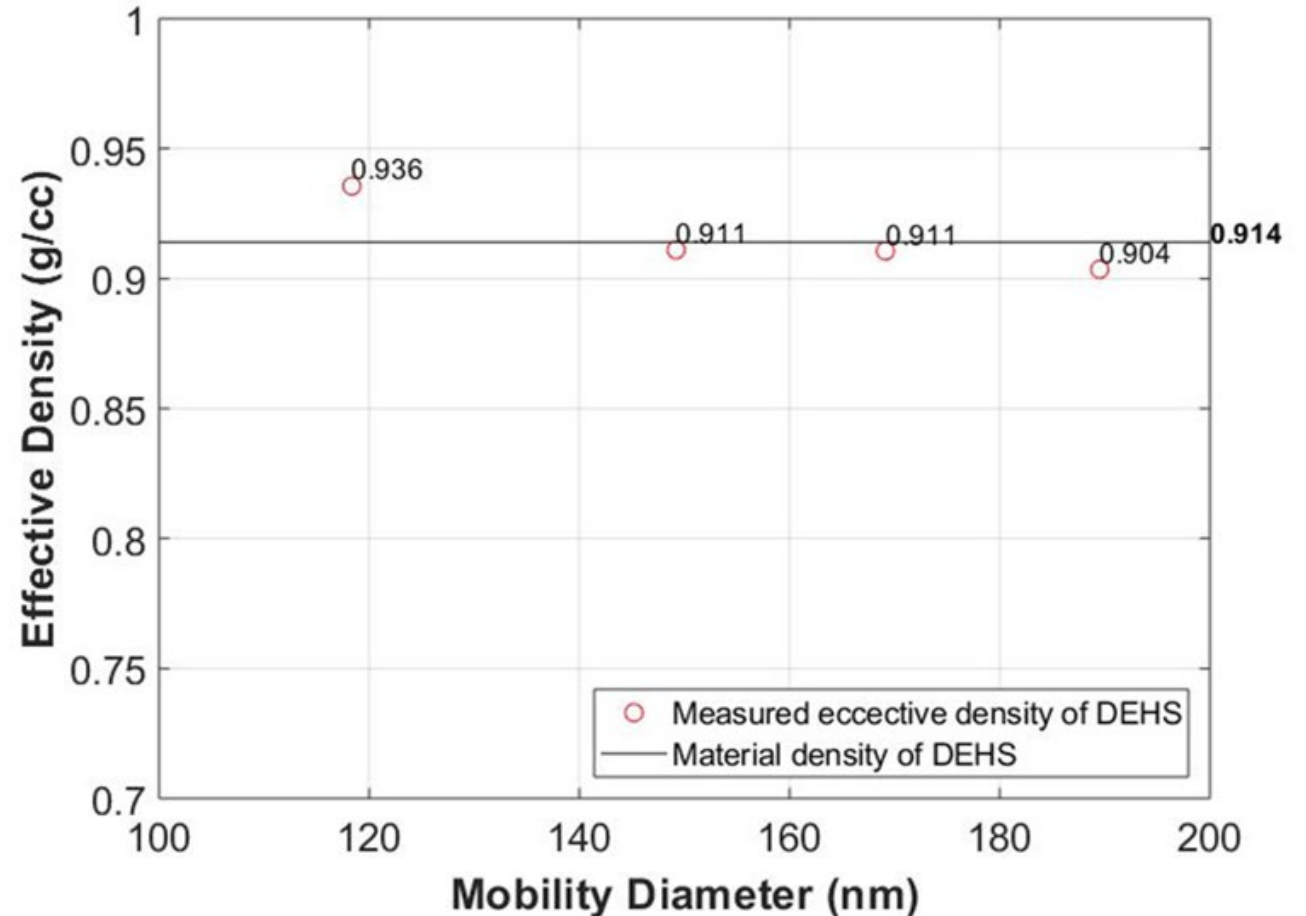
# Example of IPSD method – integrate the product of volume and density across the size distribution





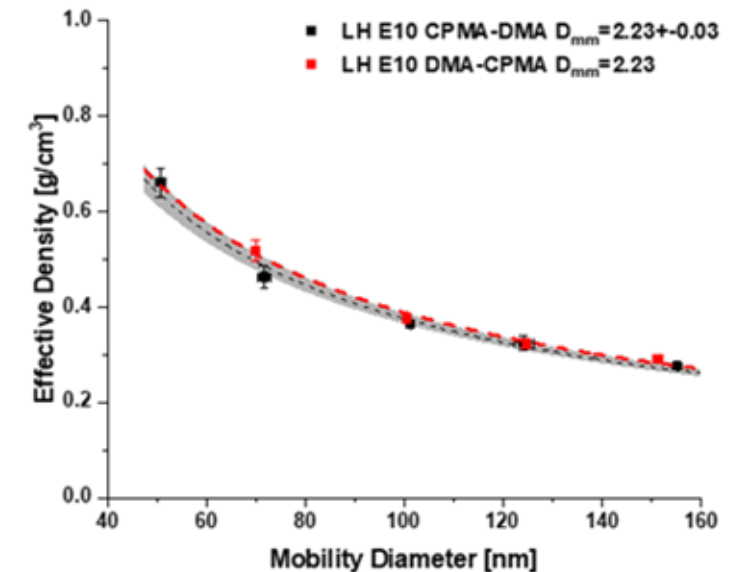
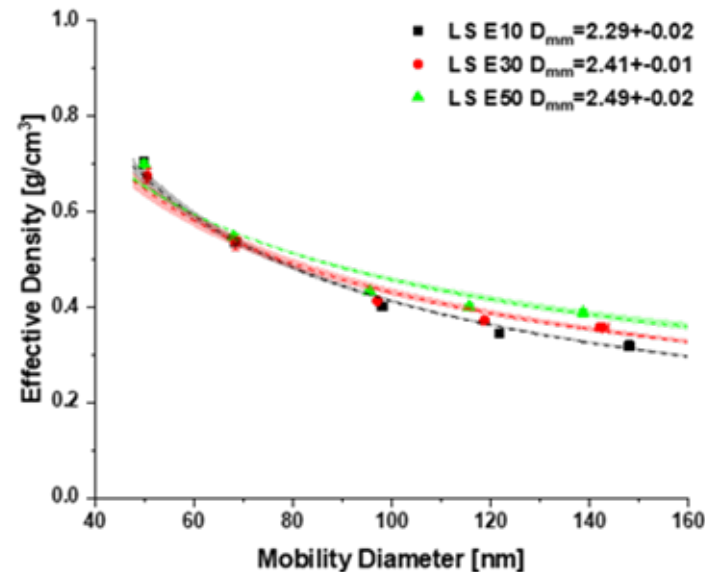
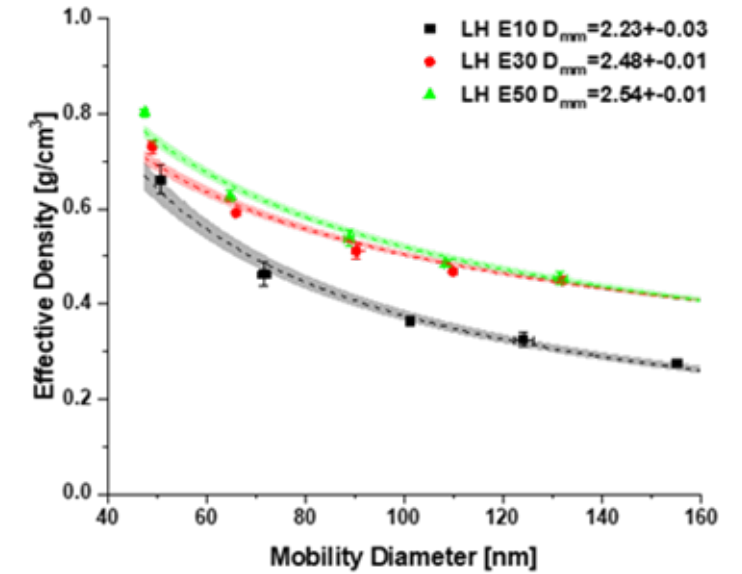
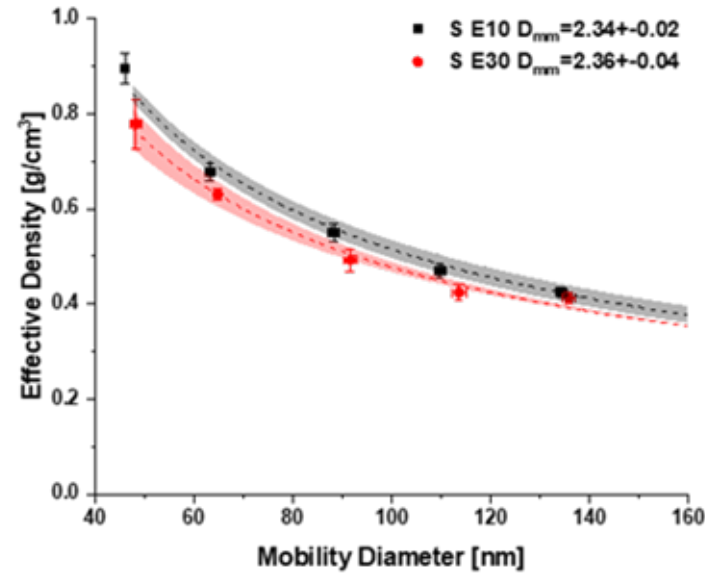
# Calibration

- CMPA and DMA calibrated against 100, 125, 152, 203 nm polystyrene latex (PSL) spheres
- Calibration checked by measuring density of Di-Ethyl-Hexyl-Sebacat (DEHS) particles,  $\rho = 0.914 \text{ g/cm}^3$
- Apparent density increase at smaller size due to evaporation



# Effective densities of non-volatile soot particles

- Fuels: E10, E30, E50
- S=stoichiometric 2000 RPM 7bar BMEP
- LH=Lean homogenous 2000 RPM 7bar BMEP
- LS=lean stratified 2000 RPM 4bar BMEP
- Shaded areas uncertainty bands
- CPMA-SMPS and DMA-CPMA-CPC configurations, **lower right panel**, agree within experimental error ( $\pm 3\%$ )



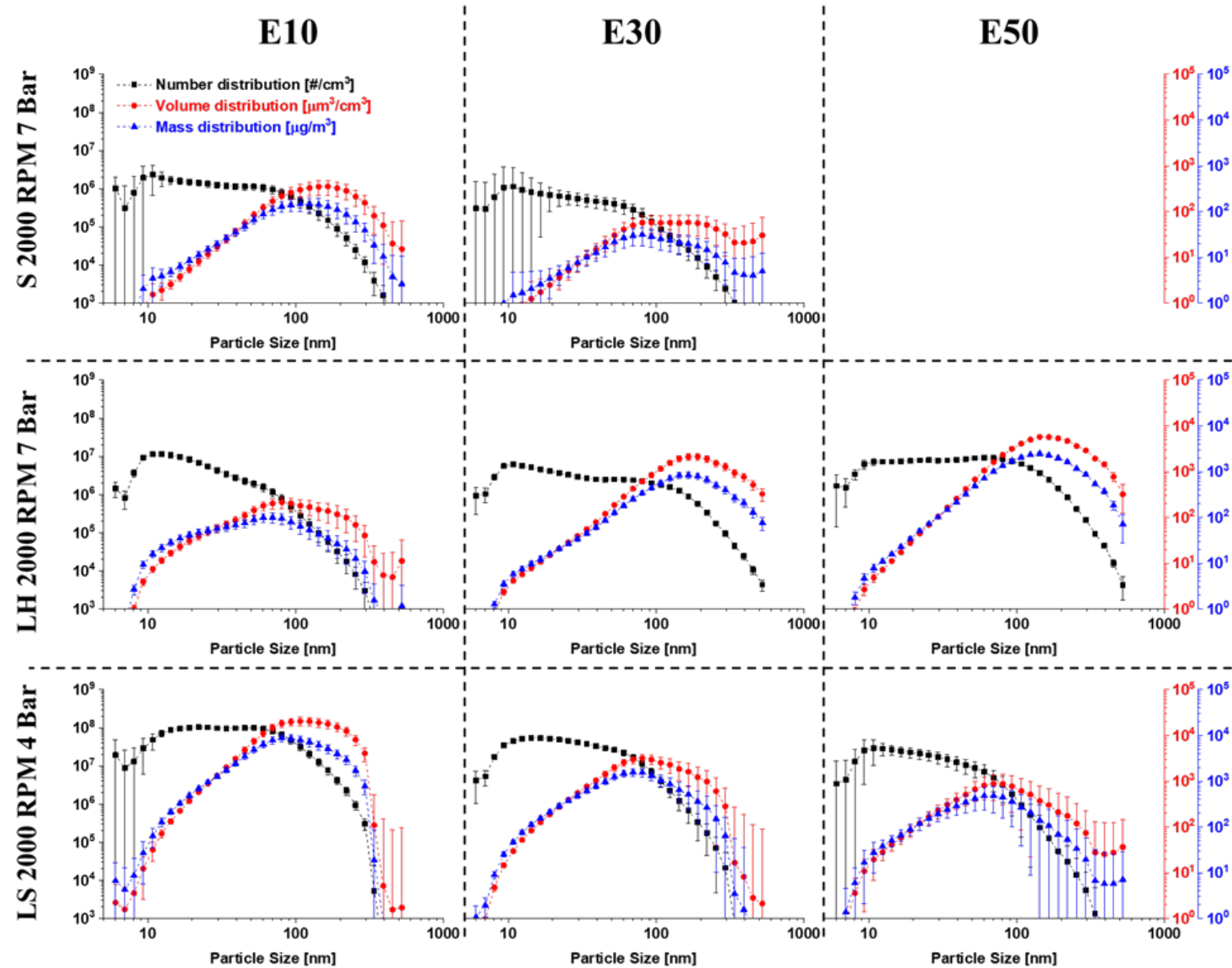
Summary of Effective Density Measurements for GDI Engines									
Study	Condition	Aftertreatment	Sample treatment	Method	Fuel	Constant	D <sub>mm</sub>	D <sub>p</sub> [nm]	rho [g/cm <sup>3</sup> ]
Graves et al., 2017 [24] , 1 engine, engine dyno	Average of Idle, 4%, 13%, 26%	3-way cat	Thermal denuder	DMA-CPMA	E0	5.22	2.49	100	0.50
	Average of Idle, 4%, 13%, 26%				E10	5.54	2.48	100	0.51
	Average of Idle, 4%, 13%, 26%				E50	5.95	2.43	100	0.43
Quiros et al., 2015 [31] , 2 vehicles, chassis dyno	Average moderate load	3-way cat	None	DMA-CPMA	E10	6.00	2.45	100	0.48
	Average high load				E10	14.00	2.30	100	0.56
Momenimovahed and Olfert, 2015 [32], Average of 5 vehicles, chassis dyno	Average 60 kph, 0, 5, 10% rated power	3-way cat	Thermal denuder	DMA-CPMA	Commercial gasoline	3.22	2.61	100	0.52
	Average 60 kph, 0, 5, 10% rated power		None			4.28	2.56	100	0.57
Symonds et al., 2008 [add] , 1 engine, engine dyno	1000 rpm, 3.27 Bar BMEP	3-way cat	None	DMA-CPMA	EN228:2004 compliant gasoline	3.29	2.65	100	0.66
Maricq and Xu, 2004 [30] , 1 vehicle, chassis dyno	Average 20, 40, 50, 60, 70 kph	3-way cat	None	DMA-ELPI	Indolene clear (E0)	15.70	2.30	100	0.63
Zelenyuk et al., 2014 [43], 1 engine, engine dyno	High load average 2000-2500 rpm 5.5 bar BMEP	None	None	APM-SMPS		38.81	2.17	100	0.83
	Low load average 2000 rpm 14 bar BMEP					38.43	2.21	100	1.01
Zelenyuk et al., 2017 [10], 1 engine, engine dyno	Stoichiometric 2000 rpm 2 Bar BMEP	3-way cat	None	APM-SMPS	E0	NA	2.10	NA	NA
	Lean stratified 2000 rpm 2 Bar BMEP					47.88	2.12	100	0.83
This study, 1 engine, engine dyno	Stoichiometric, 2000 rpm 7 Bar BMEP	None	Catalytic stripper	CPMA-SMPS	E10	10.94 ± 0.55	2.34 ± 0.02	100	0.52
	Stoichiometric, 2000 rpm 7 Bar BMEP				E30	9.25 ± 1.76	2.36 ± 0.04	100	0.49
	Lean homogeneous, 2000 rpm 7 Bar BMEP			DMA-CPMA	E10	13.52	2.23	100	0.39
	Lean homogeneous, 2000 rpm 7 Bar BMEP			CPMA-SMPS	E10	13.42 ± 1.92	2.23 ± 0.03	100	0.39
	Lean homogeneous, 2000 rpm 7 Bar BMEP				E30	4.13 ± 0.25	2.54 ± 0.01	100	0.50
	Lean homogeneous, 2000 rpm 7 Bar BMEP				E50	5.59 ± 0.22	2.48 ± 0.01	100	0.51
	Lean stratified, 2000 rpm 4 Bar BMEP				E10	10.65 ± 0.99	2.29 ± 0.02	100	0.40
	Lean stratified, 2000 rpm 4 Bar BMEP			E30	6.39 ± 0.30	2.41 ± 0.01	100	0.42	
Lean stratified, 2000 rpm 4 Bar BMEP	E50	4.89 ± 0.43	2.49 ± 0.02	100	0.47				
<b>Olfert and Rogak, 2019</b>	<b>Universal effective density distribution</b>					<b>5.59 ± 0.09</b>	<b>2.48 ± 0.02</b>	<b>100</b>	<b>0.51</b>

# Summary of Density Measurements, GDI Engines

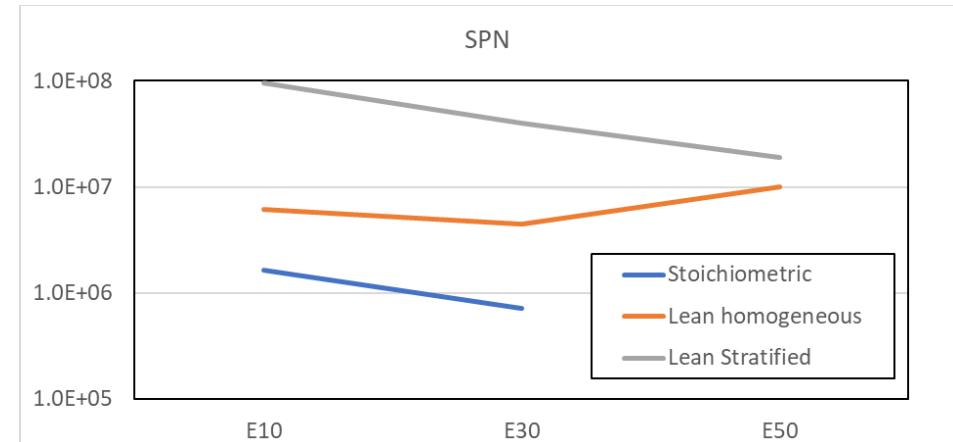
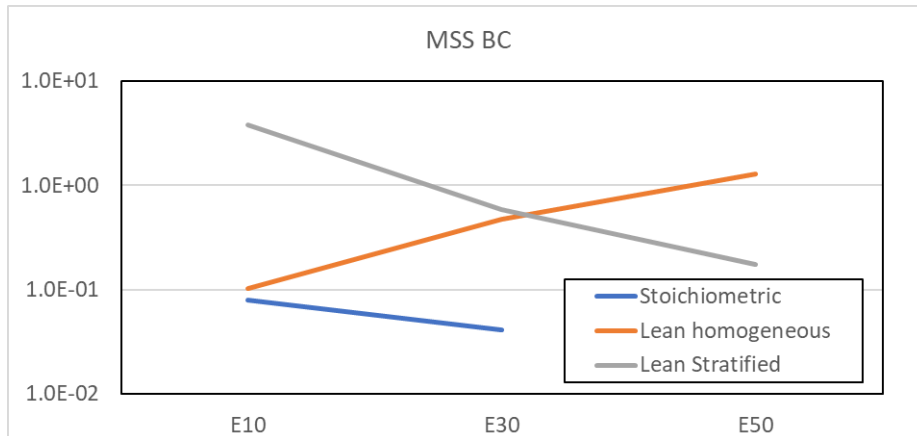
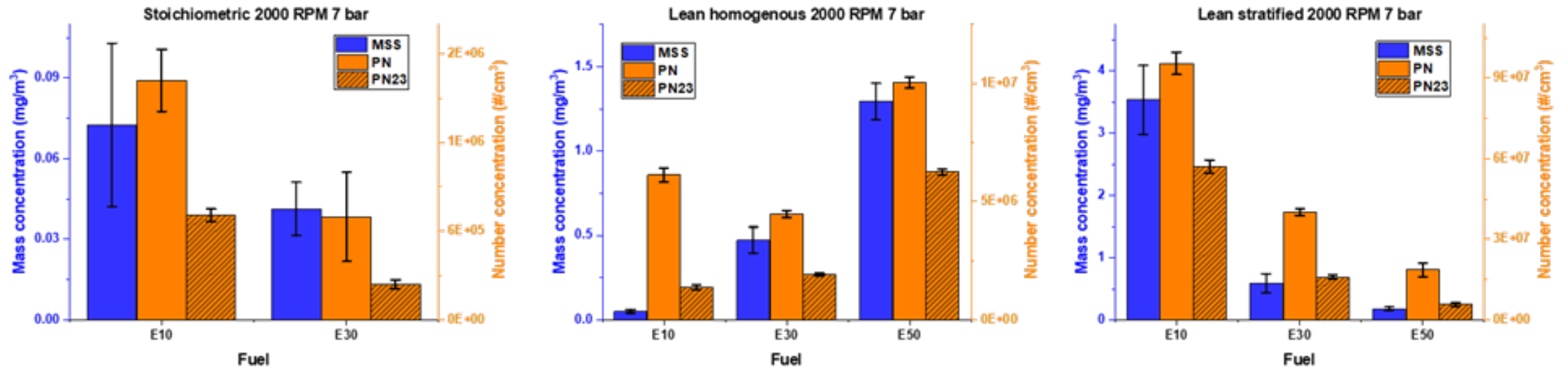
$$\rho_{eff} = Cd_m^{Dmm-3}$$

Sample treatment	C	Dmm	density eff @ 100 nm
undenuded <sup>1</sup>	8.7 ± 5.8	2.45 ± 0.16	0.58 ± 0.07
denuded <sup>2</sup>	5.0 ± 1.2	2.5 ± 0.07	0.49 ± 0.04
<b>This study - catalytic stripper</b>	8.2 ± 3.4	2.39 ± 0.11	0.46 ± 0.05
<b>Olfert and Rogak - universal (denuded)<sup>3</sup></b>	5.59 ± 0.09	2.48 ± 0.02	0.51
<b>Diffusion limited Cluster Aggregate<sup>4</sup></b>		2.2	

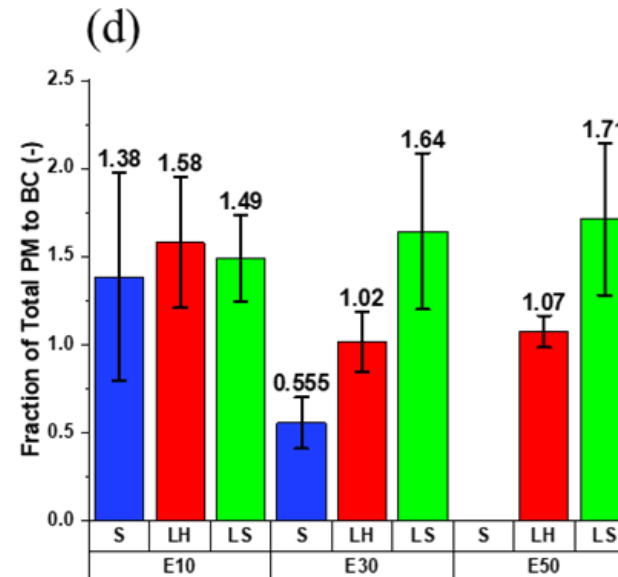
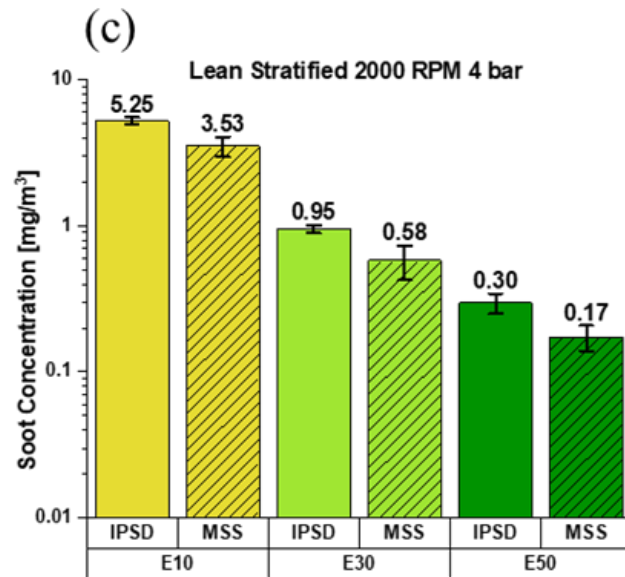
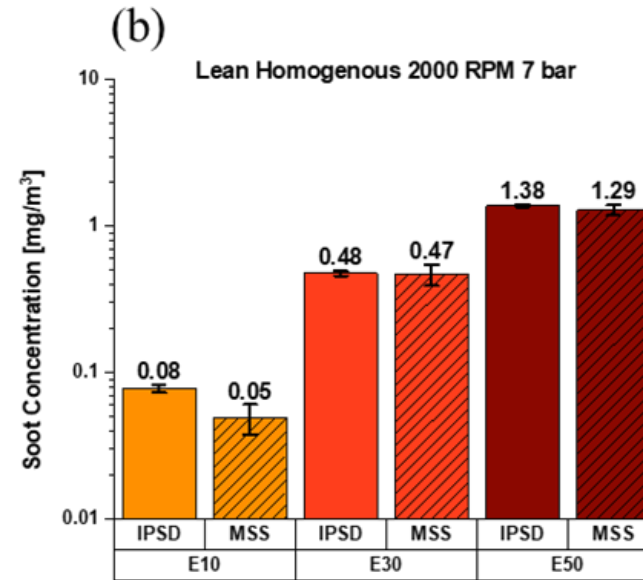
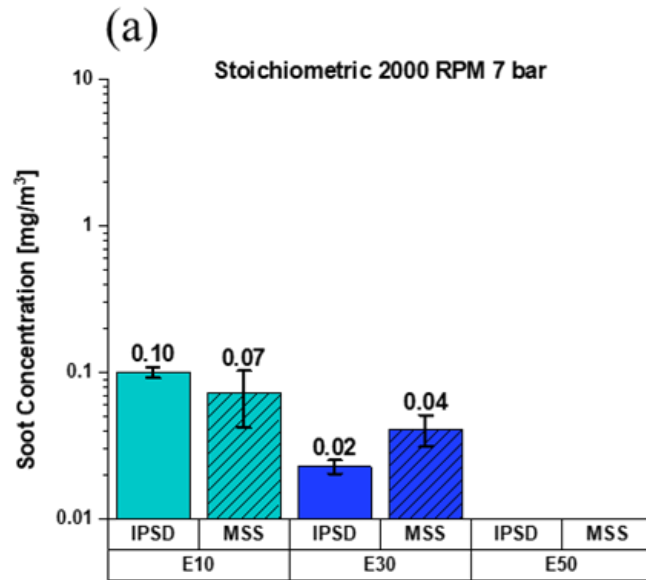
# Non-volatile particle size distributions (EEPS)



SPN23 and SPN (solid particle number > 23 and >6 nm, respectively) and MSS black carbon mass



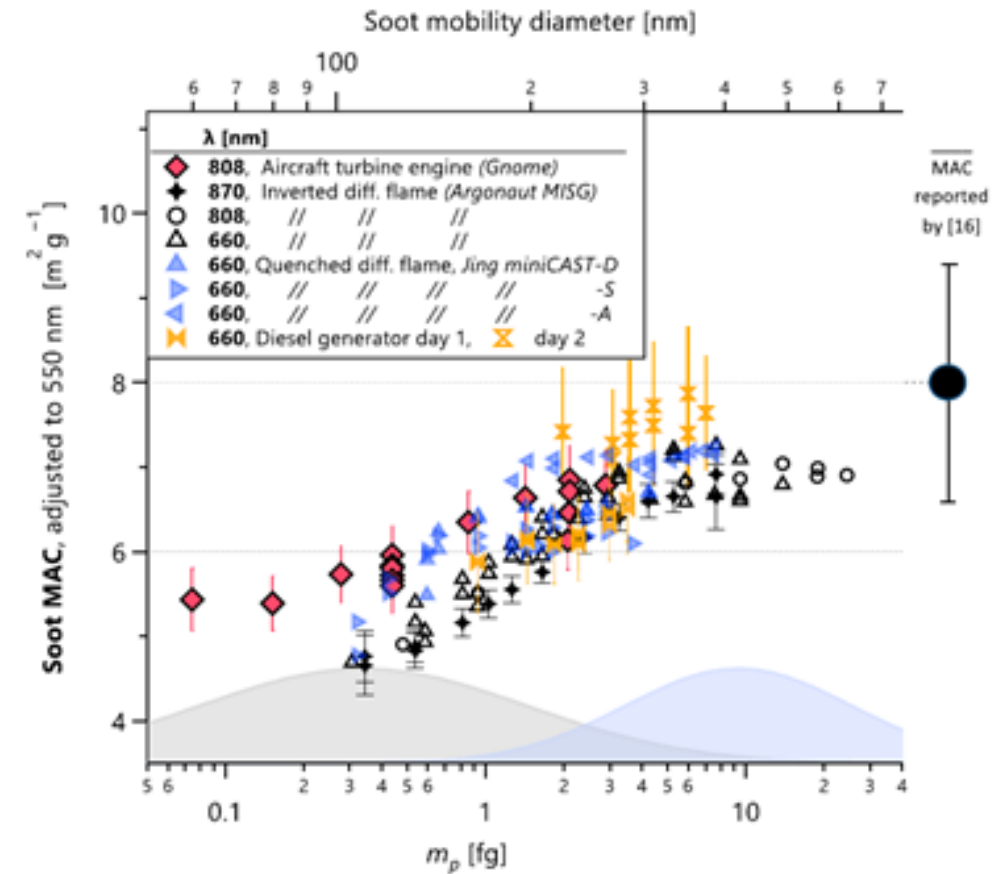
# Comparison of BC mass and IPSD mass



# Comparison of BC mass and IPSD mass

For most of our tests IPSD mass is larger than MSS BC mass, with IPSD/MSS averaging about 1.3 but with values as high as 1.7 for the LS condition, why?

- These ratios are higher than recently reported for GDI vehicles.
  - Xue, et al., 2016, 4 vehicles, IPSD/MSS = 1.01 to 1.18, average 1.06
  - Maricq. et al., 2016, 6 vehicles, IPSD/MSS average = 1.35
- IPSD mass includes all PM, soot, heavy semi-volatiles, ash
- MSS mass includes only black carbon
  - MSS mass assumes light mass absorption cross section (MAC) is the same as calibration source
  - Corbin, et al., 2022, show significant dependence of MAC on combustion conditions, particle size
  - Maricq, 2014 reports low BC/EC ratio, MAC, for immature soot
  - Malmborg, et al., 2021, reports immature soot in high EGR Diesel
  - Injection strategy used with LS mode may produce lower MAC soot



From Corbin, et al., 2022



# Summary

- Effective densities of particles from GDI engines fall in relatively narrow range
- The “universal form” is reasonable approximation in the absence of direct measurements

$$\rho_{eff} = 5.59 dm^{(2.48-3)}$$

- Fuel ethanol content strongly influences SPN and BC
  - Decreasing them for S and LS conditions
  - Increasing them for LH condition
- This lean burn GDI forms broad non-volatile particle size distributions with little distinct modal structure
- The ratio non-volatile IPSD mass to MSS BC mass is greater than 1, especially for the LS condition where it is 1.5-1.7, suggesting that the MAC for these particles is lower than for MSS calibration particles (CAST burner)

Thank you – questions?

# References for density measurements

<sup>1</sup> M.M. Maricq, N. Xu, The effective density and fractal dimension of soot particles from premixed flames and motor vehicle exhaust, *J. Aerosol Sci.* 35 (2004) 1251–1274. <https://doi.org/10.1016/j.jaerosci.2004.05.002>.

D.C. Quiros, S. Hu, S. Hu, E.S. Lee, S. Sardar, X. Wang, J.S. Olfert, H.S. Jung, Y. Zhu, T. Huai, Particle effective density and mass during steady-state operation of GDI, PFI, and diesel passenger cars, *J. Aerosol Sci.* 83 (2015) 39–54. <https://doi.org/10.1016/j.jaerosci.2014.12.004>.

A. Momenimovahed, J.S. Olfert, Effective Density and Volatility of Particles Emitted from Gasoline Direct Injection Vehicles and Implications for Particle Mass Measurement, *Aerosol Sci. Technol.* 49 (2015) 1051–1062. <https://doi.org/10.1080/02786826.2015.1094181>.

Symonds, J., Price, P., Williams, P. and Stone, R., 2008. Density of particles emitted from a gasoline direct injection engine. In 12th ETH conference on combustion generated nanoparticles

<sup>2</sup> B.M. Graves, C.R. Koch, J.S. Olfert, Morphology and volatility of particulate matter emitted from a gasoline direct injection engine fuelled on gasoline and ethanol blends, *J. Aerosol Sci.* 105 (2017) 166–178. <https://doi.org/10.1016/j.jaerosci.2016.10.013>.

A. Momenimovahed, J.S. Olfert, Effective Density and Volatility of Particles Emitted from Gasoline Direct Injection Vehicles and Implications for Particle Mass Measurement, *Aerosol Sci. Technol.* 49 (2015) 1051–1062. <https://doi.org/10.1080/02786826.2015.1094181>

<sup>3</sup> Jason Olfert & Steven Rogak (2019) Universal relations between soot effective density and primary particle size for common combustion sources, *Aerosol Science and Technology*, 53:5, 485-492, DOI: 10.1080/02786826.2019.1577949

<sup>4</sup> Sorensen, C. M. 2011. The mobility of fractal aggregates: A review. *Aerosol Sci. Technol.* 45(7):765–779. doi:10.1080/02786826.2011.560909.